

Indres 1 .

# Setting of Synchronism Check Phase Angle using Three-Steps Method

Sungkyunkwan University Prof. Chul-Hwan Kim

# Contents



## Power System Innovation Laboratory

- **1.** Introduction
- 2. Synchronism Check Phase Angle (SCPA)
- 3. Deriving SCPA using 3 steps method
  - 3.1 Step 1; Deriving SCPA considering System Condition
  - 3.2 Step 2; Deriving SCPA considering impact on turbine generator
  - 3.3 Step 3; Deriving SCPA considering impact on system stability
  - 3.4 Setting of SCPA using three steps

# 4. Simulation

- 4.1 Simulation system and conditions
- 4.2 Simulation result and analysis
- 5. Conclusion

# **1. Introduction**



## Power System Innovation Laboratory



Most of faults occurring in transmission system  $\rightarrow$  transient faults  $\rightarrow$  disappearing in a short time



#### Automatic reclosing :

economic and effective method to improve the reliability and transient stability of power system by reclosing the tripped line after predetermined time



#### Synchronism check checking a synchronism between two separated systems



#### **Synchronism check conditions :** (1) Difference of frequency

(2) Difference of voltage magnitude

(3) Difference of voltage phase angle (crucial one)



#### Standardized conservative setting : 20~30[deg]

But, it may be not a good idea especially where the lines are in proximity to generation plant (there might be very large angle separation between the lines)

# **1. Introduction**



## Power System Innovation Laboratory



\* Example for emphasizing necessity of synchronism check relay

Fig. 1 Transmission system in South-Central Michigan(2003)

- Tripping line between Argenta and Battle Creek  $\rightarrow$  phase angle difference of 80[deg]
- High speed autoreclosing without supervision of phase angle  $\rightarrow$  reclosing failure  $\rightarrow$  blackout



- Synchronism Check (to check the synchronism between two systems)
  - Limiting the impact associated with automatic reclosing under Live-Bus/Live-Line(LBLL) conditions
  - Three conditions (associated with the voltage phasors on either side of the open circuit breaker)
    - Difference of frequency, voltage magnitude, voltage phase angle



Fig. 2 Equivalent circuit for two systems to be reconnected



3.1 Step 1; Deriving SCPA considering system condition

- System study  $\rightarrow$  A kind of contingency study (e.g. lines out, fault, disturbance ...)
- Evaluating a range of system conditions to identify the worst potential system impact
- Important to find out a maximum possible angle under credible operating conditions!!
- Various factors should be considered in system study (as critical factors)

→ changing system conditions (e.g. angle separation)

- 1 Lines out (should be considered in automatic reclosing situation)
- 2 Generation level
- 3 Load level
- (4) Seasonal load power factor
- (5) Machines out

**Related to <u>flow of active power</u>** 

# 3. Deriving SCPA using 3 steps method



#### Power System Innovation Laboratory

## 3.1 Step 1; Deriving SCPA considering system condition (Cont.)





# **3.2 Step 2; Deriving SCPA considering <u>impact on turbine generator</u>**

- Damage on Turbine Generator
  - Caused by fault, <u>switching operation</u> and sub-synchronous resonance, etc.
  - Disturbances in electrical system  $\rightarrow$  torsional stress on turbine generator



Fig. 4 Electromagnetic coupling between mechanical system and electrical system

- IEEE Committee's recommendation (Screening guide)
  - "ΔP value equal to 0.5 per unit is considered an acceptable screening level for evaluating steady-state switching if a turbine generator is operating under the allowable load condition"
  - Phase angle difference causing over 0.5 per unit of  $\Delta P$  is not allowable when reclosing



# 3.2 Step 2; Deriving SCPA considering impact on turbine generator (Cont.)

- $\Delta P$  (sudden power change)
  - 'Power output at the instant of switching' 'initial power output of the unit'

$$\Delta P[p.u.] = \frac{P_{pre} - P_{post}}{S_{MVA}} \tag{1}$$



Shaft Torsional Torque (imposed by reclosing)

※ Generally, checking out the torque between GEN part and LP part
→ it is normally the largest one among all of torques.

Fig. 5 Shaft torque generated between GEN and LPB



# **3.2 Step 2; Deriving SCPA considering impact on turbine generator (Cont.)**

- δ<sub>2</sub> → maximum possible angle that can
   result in ΔP less than 0.5 per unit in
   reclosing the line (Screening guide)
- determined through an iterative process
   until getting δ<sub>2</sub> like the step-1
- *α* is an index for representing the degree
   of accuracy and if *α* is small, it suggests
   high accuracy of a process





# 3.3 Step 3; Deriving SCPA considering impact on system stability

- δ<sub>3</sub> → maximum possible angle which can
   make system restored normally without
   any problem on system stability
- determined through an iterative process like the step-2
- Integral Square Error (ISE) is used to check the system restored safely
  - one of the assessment methods for system performance





## 3.3 Step 3; Deriving SCPA considering impact on system stability (Cont.)

Integral Square Error (ISE)

$$ISE = \int_0^T \left( y(t) - y(\infty) \right)^2 dt \tag{2}$$

- $y(t) \rightarrow$  instantaneous angle across an open circuit breaker
- $y(\infty) \rightarrow$  convergent angle after reclosing (constant)
- y(t) is divergent  $\rightarrow$  ISE also becomes divergent (system got unstable)



# **3. Deriving SCPA using three steps method**



#### Power System Innovation Laboratory

## 3.4 Setting of SCPA using 3 steps method

- Setting of SCPA  $\rightarrow$  minimum value of angles among  $\delta_1$ ,  $\delta_2$  and  $\delta_3$
- Covering all the considerations at step-1, step-2 and step-3





#### Power System Innovation Laboratory



#### 4.1 Simulation System and Condition



- System is under LBLL condition (one line out situation)
- Open lines considered are the ones between BUS A and BUS C in both systems (154kV and 345kV)



#### Power System Innovation Laboratory

Parameter	value				
Rated Power[MVA]	246				
Number of poles	2				
Moment of inertia $[lb \cdot ft^2 \cdot 10^6]$	HP = 0.009032 IP = 0.015130 LPA = 0.083480 LPB = 0.085970 GEN = 0.084440 EXC = 0.003327				
Spring constant $[lbf \cdot ft \cdot 10^6]$	HP-IP = 10.988 $IP-LPA = 19.883$ $LPA-LPB = 29.622$ $LPB-GEN = 40.335$ $GEN-EXC = 1.6064$				
Fraction of external torque[%]	HP = 30, IP = 26, LPA = 22, LPB = 22				

#### Table 1. Parameters of the turbine generator in 154kV



#### Table 2. Parameters of the turbine generator in 345kV

Parameter	value
Rated Power[MVA]	612
Number of poles	2
Moment of inertia $[lb \cdot ft^2 \cdot 10^6]$	HP = 0.018358 $IP = 0.030748$ $LPA = 0.169690$ $LPB = 0.174740$ $GEN = 0.171634$ $EXC = 0.006762$
Spring constant $[lbf \cdot ft \cdot 10^6]$	HP-IP = 22.334 $IP-LPA = 40.414$ $LPA-LPB = 60.210$ $LPB-GEN = 81.985$ $GEN-EXC = 3.2651$
Fraction of external torque[%]	HP = 30, IP = 26, LPA = 22, LPB = 22

- \* The parameters shown in Table 1 and 2 are based on the physical dimensions of the shaft system and its material properties.
- ※ Multi-mass model should be used to determine the shaft torsional torque between masses

Fig. 12 Multi-mass model of the turbine generator used in transmission system



#### Power System Innovation Laboratory

## 4.2 Simulation Result and Analysis

#### Table 3. Simulation result in step-1 (154kV)

Factors considered in step-1																
Generation level		Load level (power factor : 98%)			Seasonal load power factor (Active power : 450MW at 98%)				Machine out (total number : 2)							
Initial angle of a-phase in generator [deg]	Maximum possible angle [deg]	Active power [MW]	Reactive power [MVAR]	Maximum possible angle [deg]	Season	Load power factor [%]	Active power [MW]	Maximum possible angle [deg]	Number of machine out	Maximum possible angle [deg]						
0	14.3	14.3     0       18.7     0	0	27.3	enring	07.6	1/18 163	31.7								
5	18.7		0	0	0	0	0	0	0	0	27.0	spring	27.0	440.105	51.7	0
10	23	- 150	3 150	30	200	summor	05.1	136 683	21.5	0	21.3					
15	27.3			150	50	20.0	summer	93.1	430.083	51.5						
20	unstable	- 300	(0)	20.4	6-11	07.9	440.001	21 7								
25	unstable		00	30.4	Tall	97.8	449.081	31./	1	29.1						
30	unstable	450	00	21.0		07.5	447 704	21.7								
35	unstable		450	90	31.8	winter	97.5	447.704	31./							

**Step-1** The more severe system condition is, the larger angle separation happens

<u>SCPA should be lower than 31.8 [deg] considering system conditions</u>



#### Power System Innovation Laboratory



Fig. 13 Simulation result in step-2 (154kV)

**Step-2** • There is no angle separation causing excessive  $\Delta P$ 

 $\rightarrow$  SCPA can be determined as any value considering damage on turbine generator

- **Step-3** Maximum possible angle in step-3  $\rightarrow$  31[deg]
  - $\rightarrow$  SCPA can be determined as value below 31[deg]



#### Power System Innovation Laboratory

## 4.2 Simulation Result and Analysis (Cont.)

Comparison between simulation result and conventional SCPA in Korea



Fig. 14 Comparison between SCPA of 3 steps method and conventional one (154kV)

- Results in 154kV transmission system
  - **Possibility to make the phase angle setting higher** than the angle which is used currently



#### Power System Innovation Laboratory

#### Table 5. Simulation result in step-1 (345kV)

Factors considered in step-1											
Generation level Load leve		el (power factor : 98%)		Seasonal load power factor (Active power : 450MW at 98%)				Machine out (total number : 8)			
Initial angle of a-phase In generator [deg]	Maximum possible angle [deg]	Active power [MW]	Reactive power [MVAR]	Maximum possible angle [deg]	Season	Load power factor [%]	Active power [MW]	Maximum possible angle [deg]	Number of machine out	Maximum possible angle [deg]	
20	15.9	0	0	35.9	spring	annina	07.6	118 163	30.7	0	35.0
25	19.5	150	30	37.3		97.0	440.105	57.7	0	55.7	
30	23	300	60	38.6	summer		05 1	426 692	20.4	1	26 5
35	26.6	450	90	39.9		95.1	430.083	39.4		30.5	
40	30.2	600	120	unstable	fall	fall	07.0	440.001	20.0		
45	33.8	750	150	unstable			97.8	449.081	39.8	2	unstable
48	35.9	900	180	unstable	winter	07.5	447 704	20.7	2	. 11	
50	unstable	1050	210	unstable		97.5	447.704	39.7	3	unstable	

Step-1

• The more severe system condition is, the larger angle separation happens

<u>SCPA should be lower than 39.9 [deg] considering system conditions</u>



#### Power System Innovation Laboratory



Table 6. Simulation result in step-3 (345kV)

Fig. 15 Simulation result in step-2 (345kV)

 There is limitation of angle separation causing excessive ΔP (32[deg]) Step-2

→ SCPA should be lower than 32[deg] considering damage on turbine generator

• Maximum possible angle in step-3  $\rightarrow$  39[deg] Step-3

 $\rightarrow$  SCPA can be determined as value below 39[deg]



#### Power System Innovation Laboratory

## 4.2 Simulation Result and Analysis (Cont.)

Comparison between simulation result and conventional SCPA in Korea



Fig. 17 Comparison between SCPA of 3 steps method and conventional one (345kV)

- Results in 345kV transmission system
  - conventional synchronism-check phase angle setting in Korea is quite appropriate and reasonable

# **5.** Conclusion



### Power System Innovation Laboratory

Setting of Synchronism Check Phase Angle in Transmission Line using System Condition and Damage on Turbine Generator

## • Synchronism check

- : checking a synchronism between two separated system
- 3 steps method is used by considering follows at each step
  - System condition  $\rightarrow$  evaluate a range of system conditions
  - **Damage on turbine generator**  $\rightarrow$  using  $\Delta P$  as a screening parameter
  - System stability  $\rightarrow$  using ISE to check stability of system
- Conventional SCPAs in Korea are evaluated
  - $154kV \rightarrow$  possibility to make conventional SCPA higher
  - 345kV → appropriate and reasonable

# Reliable SCPA → Solving the problems due to impacts on system



# Thank you for listening!

