



# Stability and Stabilization of Large DCPPS Through Partial Spectral Discretization-based Eigen-Analysis

#### Hua Ye Shandong University, China

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#### 1. Introduction

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### **1. Introduction**



\* As of 2012, over **2400** PMUs deployed in 500 kV and higher plants & substations of China.

\* Source: Lu C, Shi B, Wu X, et al. Advancing China's smart grid: Phasor measurement units in a wide-area management system. *IEEE Power and Energy Magazine*, 2015, 13(5): 60-71.



\* As of 03/31/2013, there were **1126** PMUs installed in US. \* Source: Department of Energy. Synchrophasor Technologies and their Deployment in Recovery Act Smart Grid Programs, August 2013.

- Thousands of phasor measurement units (PMUs) have been deployed in the transmission level all over the world, which provide a new measure for measuring, monitoring and control of the physical power system.
- Especially, wide-area damping controllers (WADCs) can effectively stabilize both local and interarea low frequency oscillations.

### Background



- Since remote signals are employed as feedback signals, time delay in the range of tens to hundreds of millisecond emerges in transmission and process of wide-area measurements.
- With the consideration of time delay effects, the cyber-physical power system (CPPS) had been involved into a *Delayed CPPS* (*DCPPS*)
- Time delays compromise the performance of wide-area control system and thus may jeopardize the stability of DCPPS.

## **DCPPS** modeling

Structure of the DCPPS:



The dynamics of the DCPPS can be represented by the following linearized delayed differential equations (DDEs):

$$\begin{cases} \Delta \dot{\mathbf{x}}(t) = \tilde{\mathbf{A}}_0 \Delta \mathbf{x}(t) + \sum_{i=1}^m \tilde{\mathbf{A}}_i \Delta \mathbf{x}(t - \tau_i), \ t \ge 0\\ \Delta \mathbf{x}(t) = \boldsymbol{\varphi}, \ t \in [-\tau_{\max}, 0] \end{cases}$$

where  $\tau_i$  (*i*=1, ..., *m*) are delay constants.

- The most popular methods to deal with DCPPS are: 1) delay-dependent stability criteria; 2) Padé approximation.
- Delay-dependent stability criteria
  - They are sufficient conditions for asymptotic stability and inherently *conservative*.
  - The scalability is constrained by the solution of the algebraic Riccati equation (ARE), where only system with less than 100 order can be dealt with.
- Padé approximation
  - Low order Padé approximation results in major phase estimating errors in the case of large time delay.

### Inertial block vs. Exponential delay term



Figure (a) Magnitude responses for inertial block and exponential delay term when delays are 0.05 and 0.1s.

Figure (b) Phase responses for inertial block and exponential delay term when delays are 0.05 and 0.1s.

#### The inertial block leads to *major* magnitude and phase estimating errors.

- 1. The inertial block results in magnitude estimating errors of 2.09 and 5.4 db when delays are 0.05 and 0.1 s, respectively.
- 2. The inertial block results in phase estimating errors of 6.85 and 32.48 degrees when delays are 0.05 and 0.1 s, respectively.

### Padé approximation vs. Exponential delay term



Figure (a) Phase responses of Padé approximation with orders of 2-4 when the delay is equal to 150ms.



Figure (b) Trajectory of the inter-area oscillation mode of the two-area four-machine test system w.r.t. delay = 0.02, 0.05, 0.1, 0.2:0.2:2.0s.

# Low order Padé approx. results in *major* phase estimating errors in the case of *large* time delays.

- When delay equal to 0.15s, the phase estimating errors for Padé approximation with orders of 2-4 are 4.04, 0.18 and 0.09 degrees, respectively.
- When delay increases to 0.5s, errors for Padé approximation with orders of 3 and 5 are 32.35 and 1.16 degrees, respectively.

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### 2. Spectral discretization-based eigen-analysis

The characteristic equation of DCPPS is:

$$\left(\tilde{A}_{0}+\sum_{i=1}^{m}\tilde{A}_{i}e^{-\lambda\tau_{i}}\right)v=\lambda v$$

where  $\lambda$  and  $\mathbf{v}$  are the eigenvalue and the corresponding right-eigenvector.

#### Challenges

- Since the exponential delay terms are involved, the characteristic equation is *transcendental* in nature.
- The equation has an infinite number of eigenvalues, which is basically unsolvable by traditional eigenvalue methods.

#### Our solution

 To compute a set of the rightmost or the least damped eigenvalues of the system by using the *spectral discretization*based eigen-analysis methods.



Figure. Illustration of the spectrum of DCPPS

#### Theoretical foundation

- There are only a finite number of eigenvalues in any vertical strip of the complex plane.
- The number of eigenvalues lying in the right-half complex plane are at most in a finite number.

### Principle of spectral discretization method

The spectral discretization-based eigenvalue method can compute a set of critical eigenvalues from the discretized matrices approximating the solution operator T(h) and the infinitesimal generator A.





#### Framework of spectral discretization method

Delayed differential equations (DDE) of DCPPS  $\Delta \dot{x}(t) = \tilde{A}_0 \Delta x(t) + \sum_{i=1}^m \tilde{A}_i \Delta x(t - \tau_i)$ 

#### Semi-group operators

- 1. Solution operator  $\mathcal{T}(h)$
- 2. Infinitesimal generator  $\ensuremath{\mathcal{A}}$

Functional equations (ordinary functional equations, ODE)  $\Delta x_h = \mathcal{T}(h)\varphi$  $\Delta \dot{x}_h = \mathcal{A}\Delta x_h$ (1) Spectral mapping  $\lambda \in \sigma(\mathcal{A})$  $\lambda = \frac{\ln \mu}{h}, \mu \in \sigma(\mathcal{T}(h)) \setminus \{0\}$  (2) Spectral discretization (3) Spectral estimation  $\bigcup \hat{\lambda} = \sigma(\mathcal{A}_N), \ \bigcup \hat{\mu} = \sigma(\mathcal{T}_N)$ (4) Spectral correction (Newton iteration)  $\hat{\lambda} \to \lambda, \ \hat{\mu} \to \mu$ 

#### **Spectral discretization-based eigenvalue algorithms**

Lots of numerical methods, such as pseudo-spectral differencing (PS), linear multi-step (LMS) and implicit Runge-Kutta (IRK), can be utilized to discretize the solution operator T(h) and infinitesimal generator A.

#### Table. Spectral discretization-based eigenvalue algorithms for large DCPPS

	Pseudo-spectral (PS)	Linear multi-step (LMS)	Implicit Runge- Kutta (IRK)
Infinitesimal generator ( $\mathcal{A}$ )	IGD-PS (IIGD) IGD-PS-II (EIGD)	IGD-LMS	IGD-IRK
Solution operator $(\mathcal{T}(h))$	SOD-PS SOD-PS-II	SOD-LMS	SOD-IRK

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#### 3. Partial spectral discretization-based eigenvalue computation method

#### Motivation

- The dimension of discretized matrices  $A_N$  and  $T_N$  approximating A and T(h) is (N+1)n, which is N+1 times of the number of system state variables, resulting in excessive CPU time consumption.
- The computational burden can be reduced and the efficiency can be improved by reducing the dimension of  $A_N$  and  $T_N$ .
- Basic idea of partial spectral discretization
  - Considering a few number of wide-area damping controllers (WADCs) are installed in power system to damp out inter-area oscillations, the state variables directly affected by communication delays are very few.
  - The dimensions of discretized matrices  $A_N$  and  $T_N$  can be significantly reduced through discretizing only the *delayed* state variables instead of *all* state variables.
  - We call this as *partial spectral discretization*.

#### State variable partitioning

The *n* system state variables are divided into two sets:  $n_1$  non-delayed variables  $\Delta x^{(1)}$  and  $n_2$  delayed variables  $\Delta x^{(2)}$ . Note that  $n_1 >> n_2$ .

 $\Delta \mathbf{x} = \begin{bmatrix} \Delta \mathbf{x}^{(1)} \\ \Delta \mathbf{x}^{(2)} \end{bmatrix} \xrightarrow{\mathbf{n}_1} \text{ non-delayed variables}$  $n_2 \text{ delayed variables}$ 



Figure. Partitioning of system state variables over the past time interval  $[-\tau_{max}, 0]$ .

$$\begin{bmatrix} \Delta \dot{\mathbf{x}}^{(1)}(t) \\ \Delta \dot{\mathbf{x}}^{(2)}(t) \end{bmatrix} = \begin{bmatrix} \mathbf{A}_{11,0} & \mathbf{A}_{12,0} \\ \mathbf{A}_{21,0} & \mathbf{A}_{22,0} \end{bmatrix} \begin{bmatrix} \Delta \mathbf{x}^{(1)}(t) \\ \Delta \mathbf{x}_{2}(t) \end{bmatrix} \\ + \sum_{i=1}^{m} \begin{bmatrix} \mathbf{0}_{n_{1} \times n_{1}} & \mathbf{A}_{12,i} \\ \mathbf{0}_{n_{2} \times n_{1}} & \mathbf{A}_{22,i} \end{bmatrix} \begin{bmatrix} \Delta \mathbf{x}^{(1)}(t - \tau_{i}) \\ \Delta \mathbf{x}^{(2)}(t - \tau_{i}) \end{bmatrix} \\ \begin{bmatrix} \Delta \dot{\mathbf{x}}^{(1)}(t) = \mathbf{A}_{11,0} \Delta \mathbf{x}^{(1)}(t) + \mathbf{A}_{12,0} \Delta \mathbf{x}^{(2)}(t) + \sum_{i=1}^{m} \mathbf{A}_{12,i} \Delta \mathbf{x}^{(2)}(t - \tau_{i}) \\ \Delta \dot{\mathbf{x}}^{(2)}(t) = \mathbf{A}_{21,0} \Delta \mathbf{x}^{(1)}(t) + \mathbf{A}_{22,0} \Delta \mathbf{x}^{(2)}(t) + \sum_{i=1}^{m} \mathbf{A}_{22,i} \Delta \mathbf{x}^{(2)}(t - \tau_{i}) \\ \Delta \dot{\mathbf{x}}^{(2)}(t) = \mathbf{A}_{21,0} \Delta \mathbf{x}^{(1)}(t) + \mathbf{A}_{22,0} \Delta \mathbf{x}^{(2)}(t) + \sum_{i=1}^{m} \mathbf{A}_{22,i} \Delta \mathbf{x}^{(2)}(t - \tau_{i}) \\ \end{bmatrix}$$
  
The derivative of system states does not relate to  $\Delta \mathbf{x}^{(1)}(\theta), \ \theta \in [-\tau_{\max}, 0].$ 

#### Principle of partial spectral discretization

At *t*=0, considering the derivative of system states does not relate to  $\Delta x^{(1)}(\theta)$ ,  $\theta \in [-\tau_{\max}, 0]$ , the evaluation of  $\varphi^{(1)}(\theta)$  and  $\varphi^{(2)}(\theta)$  at each discrete points  $\theta_{N,i}$  (*i*=0, ..., *N*+1) on  $[-\tau_{\max}, 0]$  has been reduced to evaluate  $\varphi^{(1)}(0)$  at  $\theta_{N,N+1}=0$  and  $\varphi^{(2)}(\theta)$  at  $\theta_{N,i}$  (*i*=0, ..., *N*+1).



#### Dimension reduction of the discretized matrix



Since  $n_1 >> n_2$ , by applying the partial spectral discretization, the dimension of the matrix  $\overline{A}_N$  approximating A has been to 1/(N+1) times of  $A_N$ .

#### The 16-machine 68-bus test system



200 state variables 448 algebraic variables  $\tau_{f1}$ =150 ms,  $\tau_{c1}$ =90 ms  $\tau_{f2}$ =70 ms,  $\tau_{c2}$ =40 ms

### Shandong power grid (*n*=1128)



#### The North China-Central China interconnected <u>system (*n*=33028)</u>



#### Numerical tests under constant delays

has been reduced to about

1/(N+1) of that in EIGD method.

Test				EIGD		PEIGD		Speed	w/o delay	
Syst.	S	Ν	r	$Dim(\mathcal{A}_N)$	N <sub>IRA</sub> / CPU Time (s)	$Dim(\overline{\mathcal{A}}_{N})$	N <sub>IRA</sub> / CPU Time (s)	up	Dim	N <sub>IRA</sub> / CPU Time (s)
System I ( <i>n</i> =200, <i>n</i> <sub>2</sub> =6)	7j	10	20	2200	9 / 0.33	260	7 / 0.15	1.71	200	10 / 0.13
	13j	10	20	2200	15 / 0.50	260	13 / 0.27	1.60	200	17 / 0.19
	7j	20	20	4200	9/0.74	320	7/0.19	3.03	200	10 / 0.13
	13j	20	20	4200	15 / 1.24	320	13 / 0.35	3.07	200	17 / 0.19
	7j	20	50	4200	9 / 4.32	320	9 / 1.00	4.32	200	9 / 0.48
	13j	20	50	4200	10/5.25	320	10/1.19	4.41	200	11 / 0.79
System II ( <i>n</i> =1128, <i>n</i> <sub>2</sub> =6)	7j	10	20	12408	5 / 1.39	1188	5 / 0.19	7.32	1128	6 / 0.13
	13j	10	20	12408	6 / 2.16	1188	6 / 0.29	7.45	1128	8 / 0.21
	7j	20	20	23688	5 / 2.55	1248	5/0.22	11.59	1128	6 / 0.13
	13j	20	20	23688	7 / 4.24	1248	7 / 0.36	11.78	1128	8 / 0.21
	7j	40	50	23688	7 / 17.32	1248	7/1.11	15.60	1128	7 / 0.79
	13j	40	50	23688	4 / 12.50	1248	4 / 0.75	15.67	1128	4 / 0.50
System III (n=80577, <i>n</i> <sub>2</sub> =6)	7j	10	20	886347	6 / 203.10	80637	6 / 23.78	8.54	80577	7 / 20.24
	7j	20	20	1692117	6 / 381.47	80697	6 / 23.82	16.01	80577	7 / 20.24
	7j	20	50	1692117	5 / 1280.47	80697	5 / 68.41	18.72	80577	6/66.44
The dimension in PEIGD method				The speed up increases CPU time for PEIGE						

with the size of the power

system.

is almost the same as

the case without delay.

#### Numerical tests under random delays



Figure. Distributions of two time delays in 1000 trials.



Table. Statistics of CPU time for one IRA

Figure. Histogram of speed up for 1000 trails

Compared with the EIGD method, the proposed PEIGD method can save 88%~94% CPU time for one implicitly restarted Arnoldi (IRA) iteration.

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#### 4. Non-smooth optimization-based WADC tuning method

#### Motivation

- The existing method aims at maximizing the least damped oscillation mode rather than the targeted inter-area oscillation modes. The obtained WADC's parameters are absolutely not optimal.
- To cope with the non-differentiable problem, intelligent optimization algorithms, such as PSO, are popular to pursuit the optimal solution, which are prone to fall into local extreme values and characterized by low computational efficiency and reliability, etc.

#### Gradient sampling-based method

- The objective function is determined as maximizing the least damping of the targeted inter-area oscillation modes associated with the WADC to be tuned.
- The mathematical optimization methods instead of intelligent optimization algorithms are utilized to derive the optimal solutions, where the gradient at non-differentiable points are obtained by gradient sampling technique.

#### **Objective function**

The objective is to maximize the least damping of the targeted inter-area oscillation modes associated with the WADCs to be tuned.

$$\max_{p} \zeta_{I}$$
s.t. 
$$\max(\operatorname{Re}(\lambda)) \leq -\alpha, \ \lambda \in \mathbb{M}_{I}$$

$$\max(\zeta(\lambda)) \leq \zeta_{0}^{i}, \ \lambda \in \mathbb{M}_{R}^{i}, i = 1, \cdots, n_{p}$$

$$\max(\operatorname{Re}(\lambda)) \leq -\alpha_{0}^{i}, \ \lambda \in \mathbb{M}_{R}^{i}, i = 1, \cdots, n_{p}$$

$$K_{s}^{\min} \leq K_{s,j} \leq K_{s}^{\max}, \ \lambda \in \mathbb{M}_{R}^{i}, i = 1, \cdots, n_{c}$$

$$T_{i}^{\min} \leq T_{i,j} \leq T_{i}^{\max}, \ \lambda \in \mathbb{M}_{R}^{i}, i = 1, 2, 3, 4$$

$$\bigcup_{k \in \mathbb{N}_{R}^{i}, i = 1, 2, 3, 4}$$

$$\bigcup_{k \in \mathbb{N}_{R}^{i}, i = 1, 2, 3, 4}$$

where,

 $\zeta_{I} := \min{\{\zeta(\lambda) \mid \lambda \in \mathbb{M}_{I}\}}$  denotes the least damping ratio of targeted inter-area modes;

 $\mathbb{M}_{\mathbb{I}}$  denotes the set of targeted inter-area oscillation modes under  $n_{p}$  operating conditions;  $\mathbb{M}_{\mathbb{R}}$  denotes the set of the remaining oscillation modes under  $n_{p}$  operating conditions.

#### Avoidance of "mode masking" problem



Figure (a) Illustration of optimal tuning of WADCs aiming at maximizing the smallest damping ratio among all oscillation modes.

Figure (b) Illustration of optimal tuning of WADCs aiming at maximizing the smallest damping ratio among the target inter-area oscillation modes.

#### Tracking the targeted inter-area oscillation modes



Figure. Principle of perturbation-based mode tracking

Let  $p^{(\ell)}$  be the parameters of WADCs and  $\lambda^{(\ell)}$  be one mode in  $\mathbb{M}_{\mathsf{I}}$  after the  $(\ell-1)$ th parameter adjustment. At the next parameter tuning,  $\lambda^{(\ell+1)}$  can be identified by the following three steps.

- 1) Estimating  $\hat{\lambda}^{(\ell+1)}$ : The estimation of  $\lambda^{(\ell+1)}$  denoted by  $\hat{\lambda}^{(\ell+1)}$  can be readily obtained by applying the matrix perturbation theory.
- 2) Paring  $\lambda^{(\ell+1)}$  with  $\hat{\lambda}^{(\ell+1)}$ : It is achieved by screening the minimum Euclidean distance  $\|\lambda^{(\ell+1)} \hat{\lambda}^{(\ell+1)}\|$ .
- 3) Determining inter-area modes in  $\mathbb{M}_{\mathsf{I}}$ : By taking  $\hat{\lambda}^{(\ell+1)}$  as a bridge,  $\lambda^{(\ell+1)}$  at the  $\ell$ th parameter tuning can be reliably track  $\lambda^{(\ell)}$  at the last parameter tuning.

The objective function can be reformulated by using the penalty function method and by recasting the max-min problem in a dual form, which is a challenging *non-convex and non-smooth optimization problem*.

$$\max_{p} J(p),$$

$$J(p) = -\zeta_{I} + k_{1} \max_{\lambda_{k} \in \mathbb{M}_{I}} \{0, \operatorname{Re}(\lambda_{k}) + \alpha\}$$

$$+ \sum_{i=1}^{n_{p}} k_{i+1} \max_{\lambda_{k} \in \mathbb{M}_{R}^{i}} \{0, \zeta_{0}^{i} - \zeta(\lambda_{k})\}$$

$$+ \sum_{i=n_{p}+1}^{2n_{p}} k_{i+1} \max_{\lambda_{k} \in \mathbb{M}_{R}^{i}} \{0, \operatorname{Re}(\lambda_{k}) + \alpha^{i}\}$$

$$+ \sum_{j=1}^{n_{c}} \omega_{j} \max\{0, K_{s}^{\min} - K_{s,j}, K_{s,j} - K_{s}^{\max}\}$$

$$+ \sum_{j=0}^{n_{c}-1} \sum_{i=1}^{4} \omega_{4j+i+n_{c}} \max\{0, T_{i}^{\min} - T_{i,j}, T_{i,j} - T_{i}^{\max}\}$$

#### Gradient sampling at non-differentiable points

• First, define *Clarke sub-differential* (i.e., generalized gradient) at a nondifferentiable point  $p^{(l)}$ :

$$\partial_{\mathbf{c}} J(\boldsymbol{p}^{(\ell)}) \coloneqq \operatorname{conv} \left\{ \lim_{\boldsymbol{p} \to \boldsymbol{p}^{(\ell)}} \nabla J(\boldsymbol{p}) \colon \boldsymbol{p} \in \mathcal{N} \right\}$$

where "conv" denotes the convex hull and  $\mathcal{N}$  is any full-measure subset of a neighborhood around  $p^{(l)}$  containing differentiable points.

• The steepest descent direction  $d^{(\ell)}$  is defined as the opposite of the vector z in the Clarke sub-differential whose norm is the smallest.

$$\boldsymbol{d}^{(\ell)} := -\arg\min_{\boldsymbol{z}\in\partial_c J(\boldsymbol{p}^{(\ell)})} \|\boldsymbol{z}\|$$



Figure. Point subset N around the non-differentiable point  $p^{(l)}$ 

# Test results

# Table. Performance comparison of optimal WADCs with different objective functions (Hz / %)

Operating condition	$\max\{\zeta_{i}\}$ (The p	roposed method)	max{min{ $\zeta_{I}$ , $\zeta_{R}$ }}					
	$f_{\rm I}$ / $\zeta_{\rm I}$	$f_{\sf R}$ / $\zeta_{\sf R}$	$f_{\rm I}$ / $\zeta_{\rm I}$	$f_{\sf R}$ / $\zeta_{\sf R}$				
1	0.48 / 13.09	1.10 / 6.20	0.49 / 6.34	0.98 / 6.34				
2	0.43 / 16.95	1.16 / 4.10	0.46 / 8.69	1.00 / 4.18				
3	0.48 / 13.41	1.16 / 4.20	0.39 / 7.52	1.00 / 4.24				
			Since $\zeta_R$ is equal to or less than $\zeta_I$ , mode masking problem occurs and the optimization process is stagnated.					

Operating conditions	The proposed method				PSO			
	Ks	<b>T</b> <sub>1</sub>	<b>T</b> <sub>3</sub>	Iterations / Time (s)	Ks	<b>T</b> <sub>1</sub>	<b>T</b> <sub>3</sub>	Iterations / Time (s)
1	56.77	4.00	0.69	82 / 47.64	56.85	4.00	0.69	200 / 217.23
2	100.0	4.00	0.78	43 / 57.13	100.0	4.00	0.78	200 / 220.30
3	100.0	4.00	0.75	50 / 83.63	100.0	4.00	0.75	200 / 235.82

#### Table. Optimal parameters of WADC and CPU time



Figure. Iteration history of objective function *J* and the least damping ratio of the targeted inter-area oscillation modes  $\zeta_{I}$ 

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### 5. Conclusion

- The spectral discretization-based eigenvalue computation method resolves a long-standing challenging problem for stability analysis of large power system with consideration of time delay impacts. A set of the rightmost or the least damped oscillation modes of the system can be efficiently computed.
- The partial spectral discretization-based method can significantly reduce the computational burden of original spectral discretization-based method by discretizing delayed state variables only. The computational efficiency can be enhanced by an order of magnitude.
- The parameters of WADC are optimally tuned by the gradient samplingbased non-smooth optimization method. Mode tracking method reliably tracks the targeted inter-area modes during the optimization process and the gradient sampling technique efficiently works out the steepest descent direction at the non-differentiable points. Since mode masking and stagnation problems are avoided and optimal solutions are obtained.

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# Thanks for your attention !