# The 4<sup>th</sup> International Symposium on Smart Grid — Methods, Tools, and Technologies Jinan, Shandong, CHINA Oct.29-30, 2021 Calculation of AC Short-Circuit Current at MMC-HVDC Converter Station

Xinjia Song, Qianhong Shi, Yipin Gong

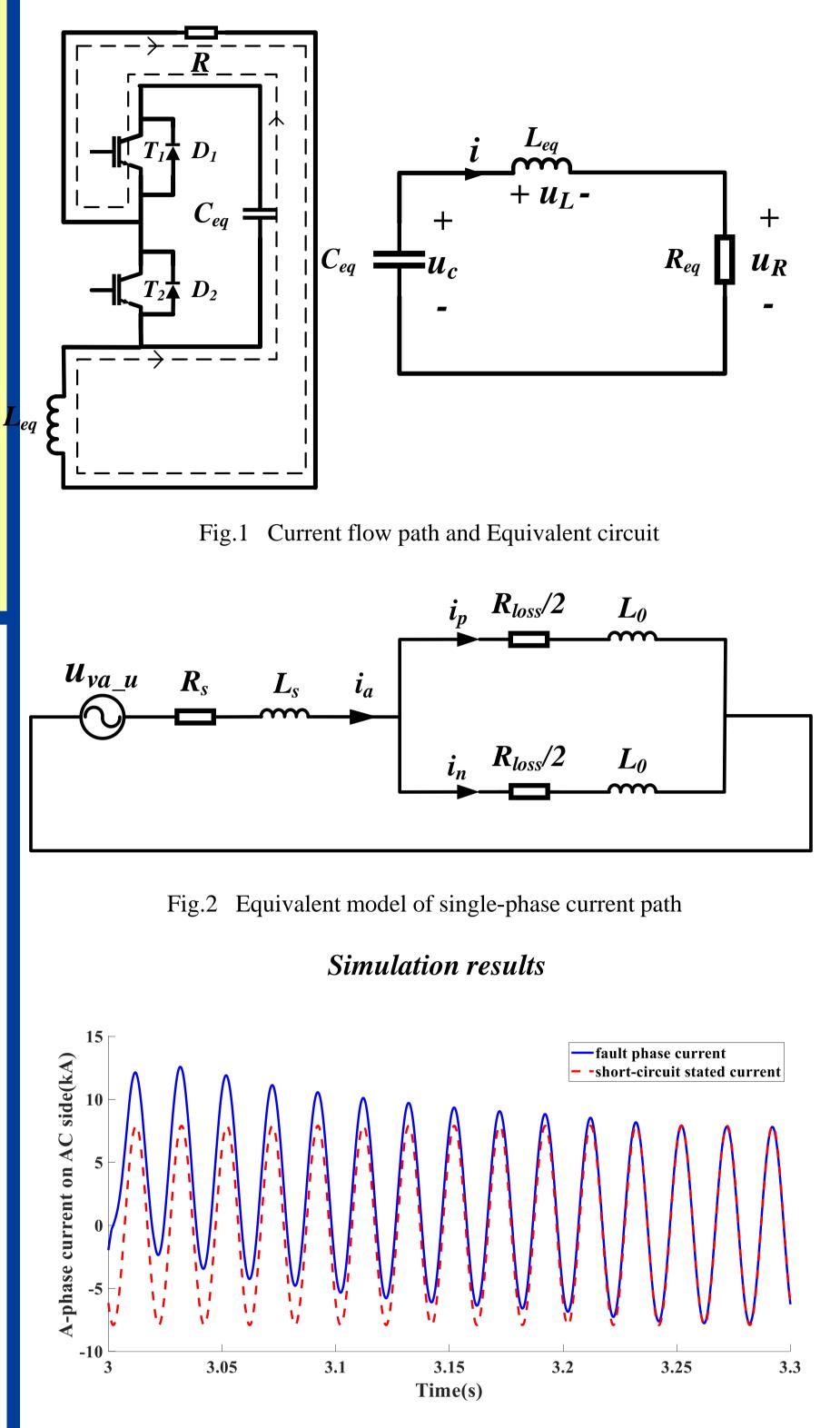
School of Electrical Engineering, Shandong University, Jinan, P.R. China

## Introduction

In recent years, Modular Multilevel Converter based High Voltage **Direct Current (MMC-HVDC)** transmission system has gradually developed, and the AC short-circuit current contributed by both the converter and AC system needs to be solved urgently. However the accurate calculation of the fault transient current is the most direct method to realize the effective evaluation of the transient process current, so providing a reference for the selection of AC side currentlimiting equipment through the accurate calculation of the shortcircuit current.

### **Method**

Fault current is divided into two parts according to the blocking time Equivalent model and current path



of converter station.

1) Equivalent model and current path before blocking

Due to symmetric bipolar structure, it can be seen that all sub-modules are involved in the discharge process. The current path and equivalent circuit of each phase is shown in Fig. 1.

Therefore, based on the principle that the energy storage capacity of the capacitor is unvaried and the second-order zero-input formula, the fault current can be obtained:

$$i = e^{-\delta t} \left[ U_{dc} \sqrt{\frac{C_{eq}}{L_{eq}}} sin(\omega t) + I_0 cos(\omega t) \right]$$

2) Equivalent model and current path after blocking

Due to the bridge arm inductance, the **inductance discharge** constitutes the DC component of the bridge arm current and **the AC system** still injects short-circuit

current to the short-circuit point.

The total current of A-phase after blocking is as follows:

Fig.3 Comparison of a-phase current simulation calculation

## Conclusions

- 1) The current path before unipolar ground fault blocking, and the short-circuit current path on the AC side after blocking.
- 2) Clarified the fault mechanism and calculation equations of the AC side short-circuit current

$$I_{a} \ s = I_{a1} \ s + I_{a2} \ s = \frac{U \ s + L_{s}i_{a-}0 + \frac{L_{0}}{2} \ i_{p-}0 + i_{n-}0}{R_{s} + sL_{s} + \frac{R_{loss}}{4} + \frac{sL_{0}}{2}}$$

After simplification, the phase a current can be rewritten:

$$I_{a} \ s = \frac{U \ s \ + \left(L_{s} + \frac{L_{0}}{2}\right)i_{a-}0}{R_{s} + \frac{R_{loss}}{4} + s\left(\frac{L_{0}}{2} + L_{s}\right)}$$

This paper builds the MMC-HVDC two-terminal 38-level power transmission system in PSCAD. Then **the total fault current of AC side** should be verified. The simulation results are shown in Fig. 3. **3)** The calculation method is verified by the two-terminal simulation model built in PSCAD.

#### References

- 1. Leterme W, Beerten J, and Hertem D V, "Equivalent Circuit for Half-Bridge MMC Dc Fault Current Contribution," Energy Conference. IEEE, 2016.
- H. Ma, W. Yao, J. Wu, D. Xing, M. Yang, S. Sun, and G. Li, "Analysis of DC Pole-to-Pole Short Circuit Fault Behavior in MMC-HVDC Transmission Systems With Bridge Arm Damper," Power System Technology ,2017,41(07):2099-2106.
- B. Li, J. He, J. Tian, Y. Feng, and Y. Dong, "DC fault analysis for modular multilevel converter-based system," Journal of Modern Power Systems & Clean Energy, 2017, 5(2):275-282.