



Towards Smarter DC Distribution Systems for Railway Applications

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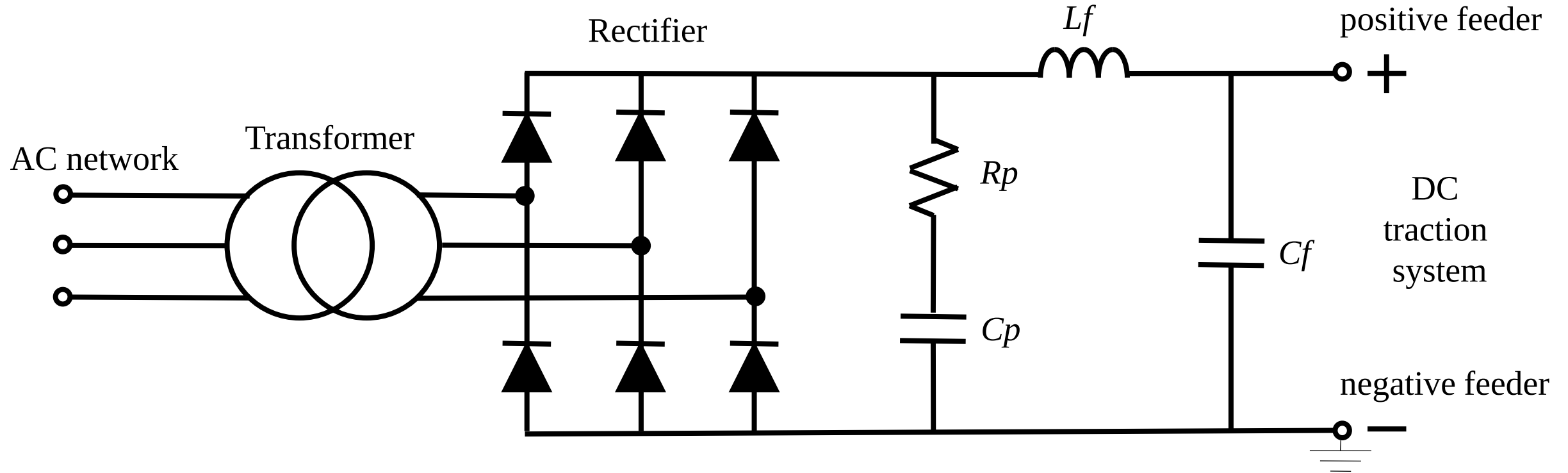
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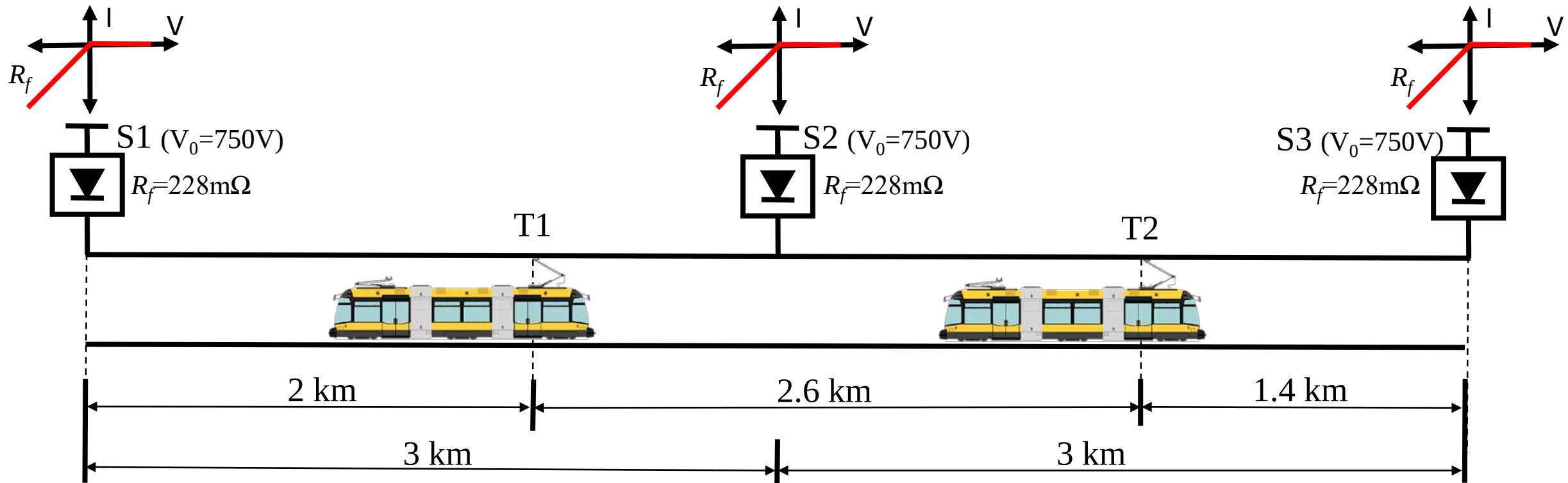
Universidad de
Oviedo

Traditional DC traction systems for light railways



Single group non-reversible conventional substation

Conventional DC scenario



Positive feeder: $R_p = 51\text{m}\Omega/\text{km}$

Negative feeder: $R_n = 14\text{m}\Omega/\text{km}$

Train max. traction and braking power (0,65MW)

Substations rated power:

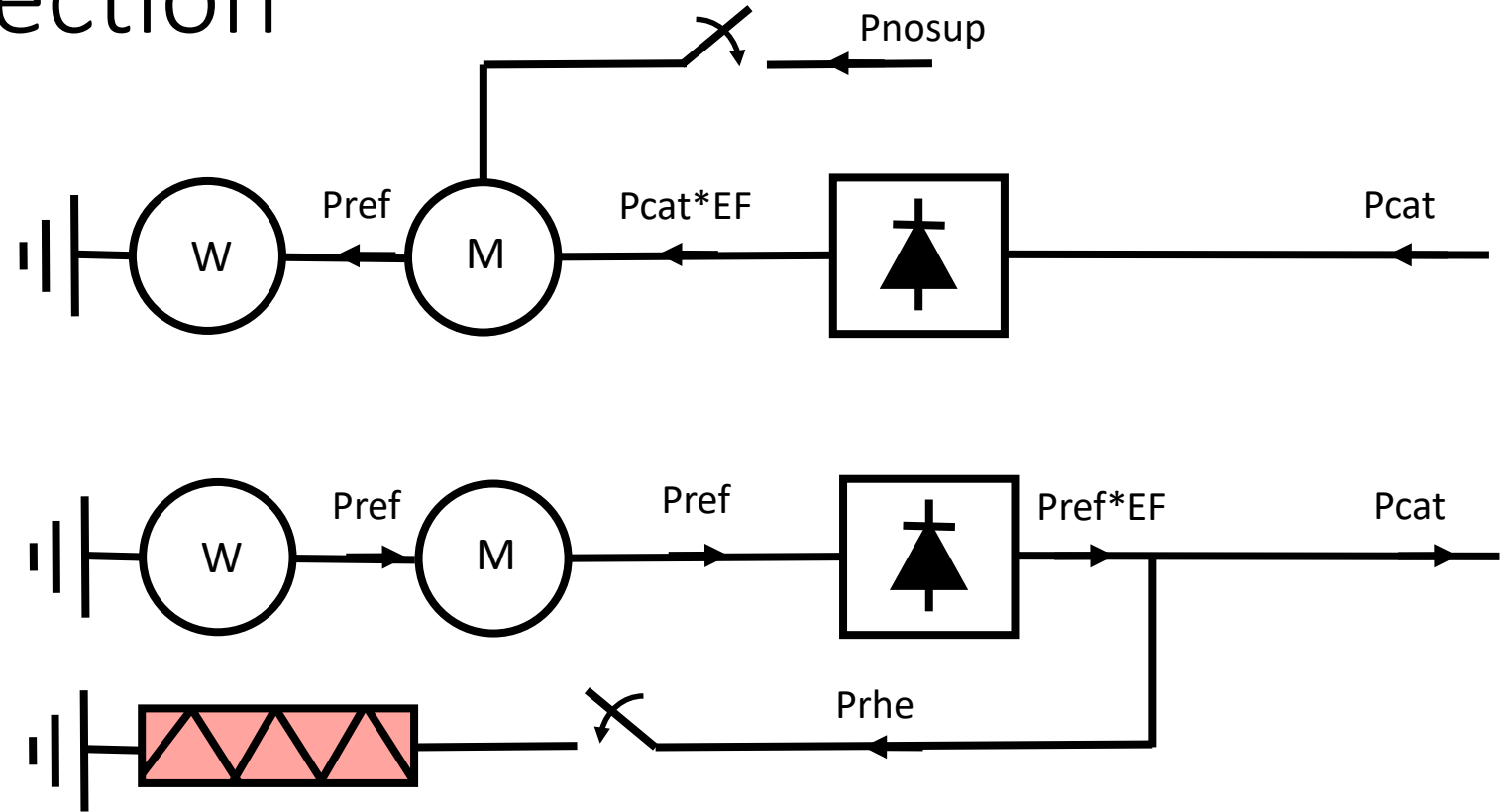
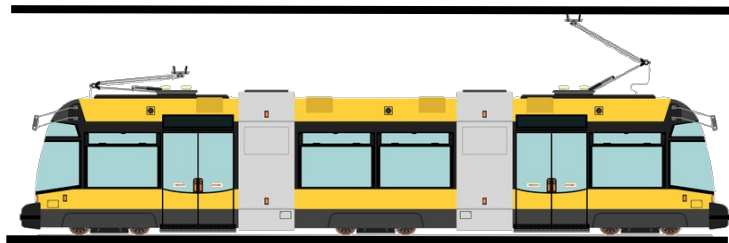
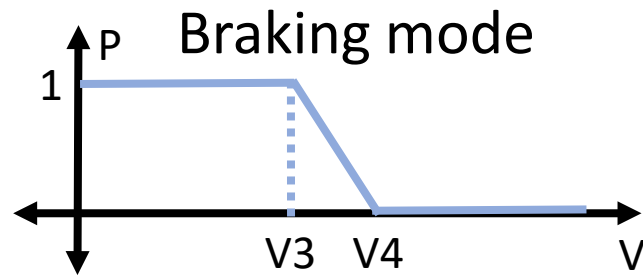
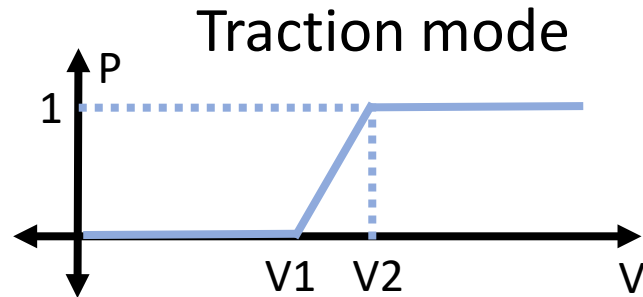
$P_r = 0,35\text{ MW}$

No load and rated load DC voltage: $V_0 = 750\text{V}$, $V_n = 700\text{V}$

Power transformer s.c. voltage:

$V_{cc} = 8\%$

Effect of the trains overcurrent and overvoltage protection



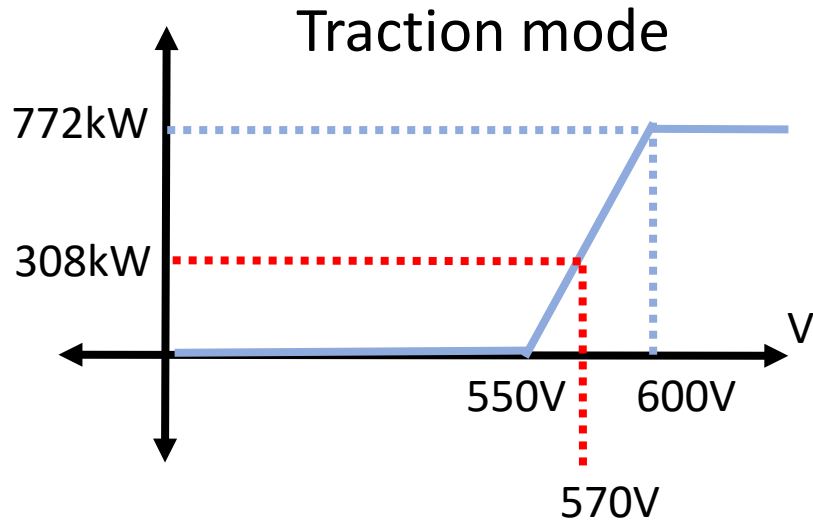
From now on it will be assumed:

Efficiency = 0.9

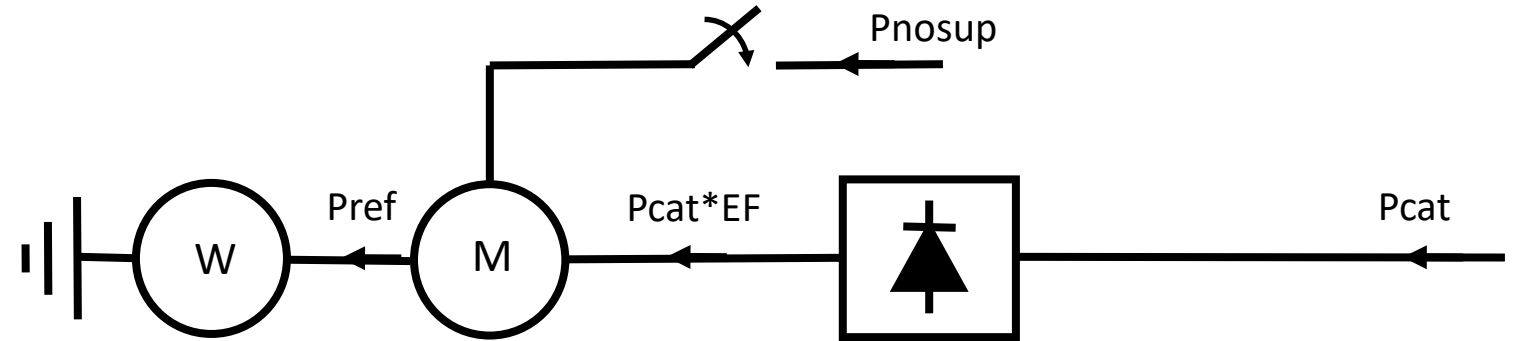
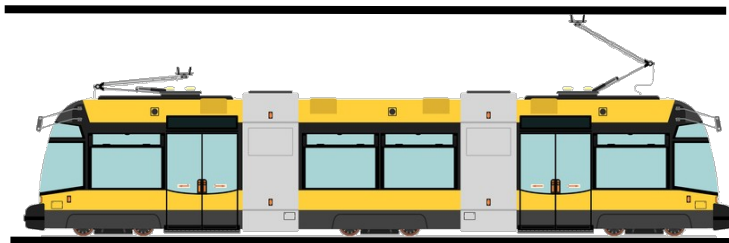
$V_1 = 550V$; $V_2 = 600V$

$V_3 = 850V$; $V_4 = 900V$

Effect of the trains overcurrent protection



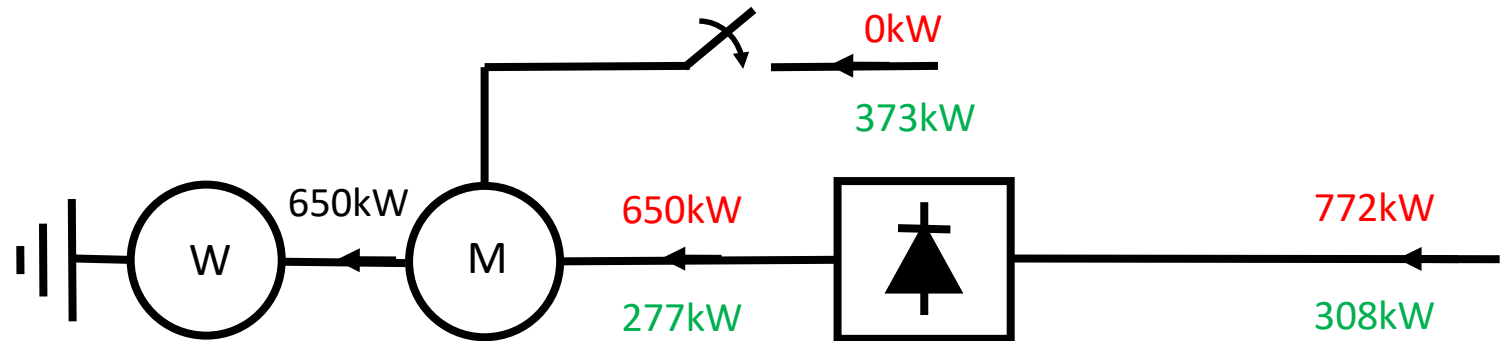
Efficiency = 0.9
 $V_1 = 550V$; $V_2 = 600V$



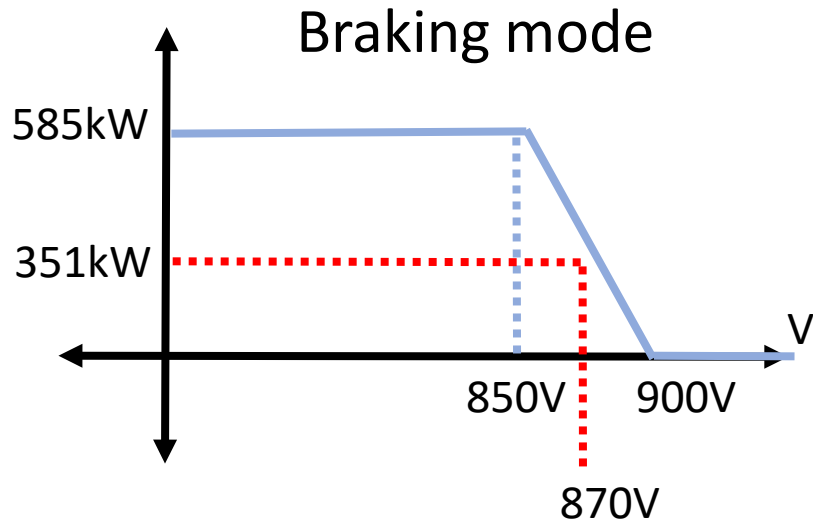
Assuming $V_{cat} = 570V$

$P_{ref} = 650kW$ $\longrightarrow$ I need from the catenary $P_{ref}/EF = 722kW$

The overcurrent protection limits the power to 308kW

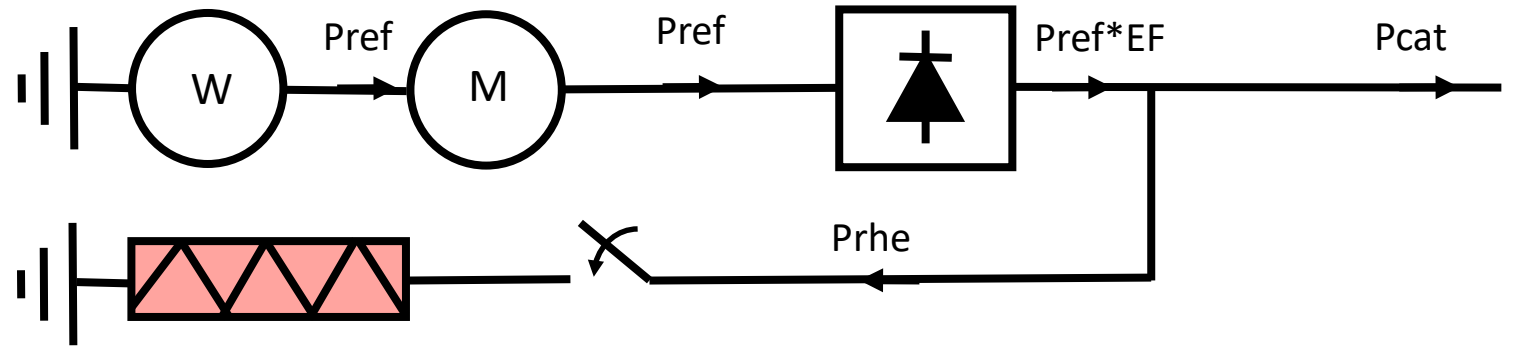
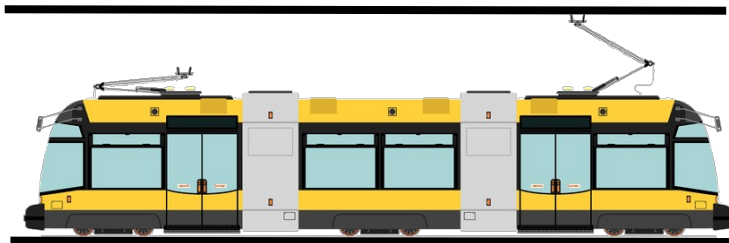


Effect of the trains overvoltage protection



Efficiency = 0.9

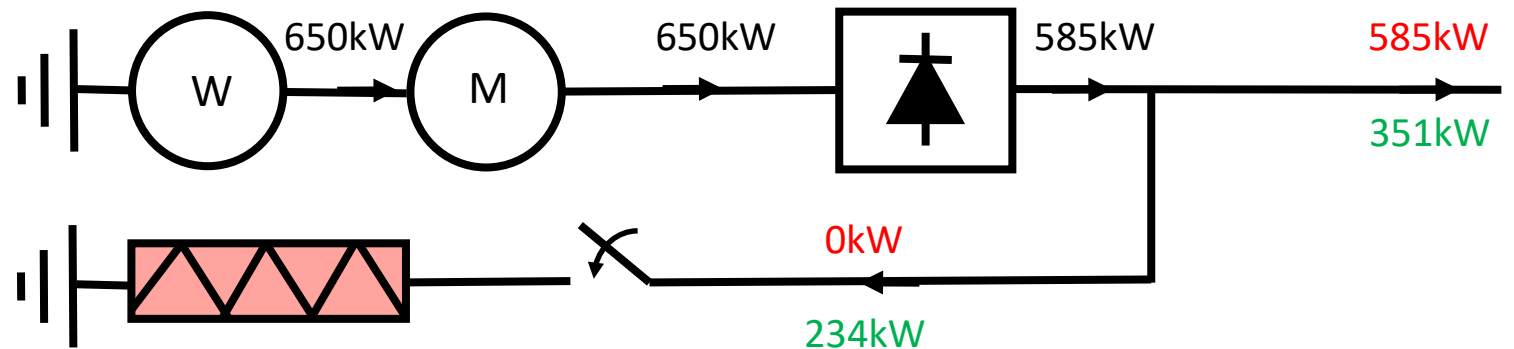
$V_3 = 850V$; $V_4 = 900V$



Assuming $V_{cat} = 870V$

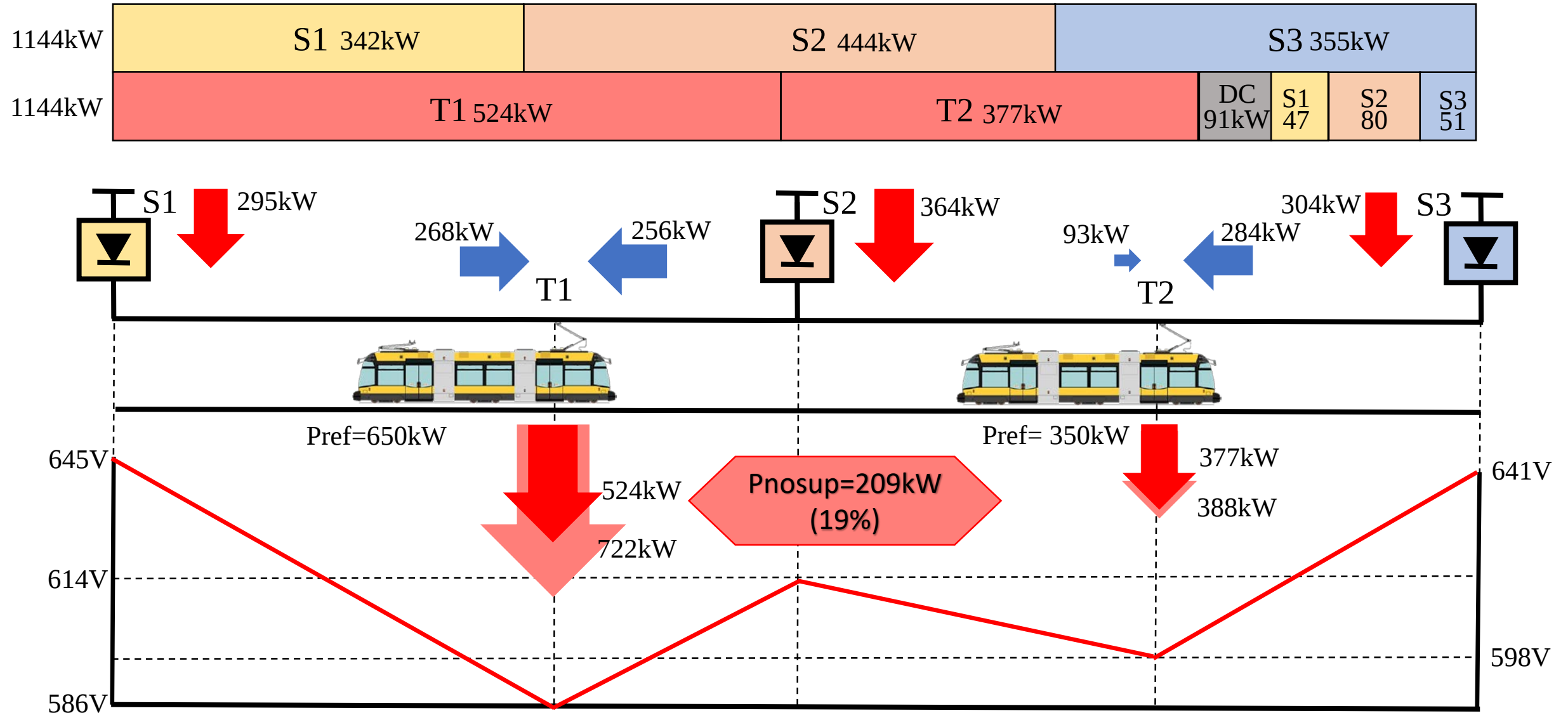
$P_{ref} = 650kW \longrightarrow$ I would like to inject in the catenary $P_{ref} * EF = 585kW$

The overvoltage protection limits the power to 351kW



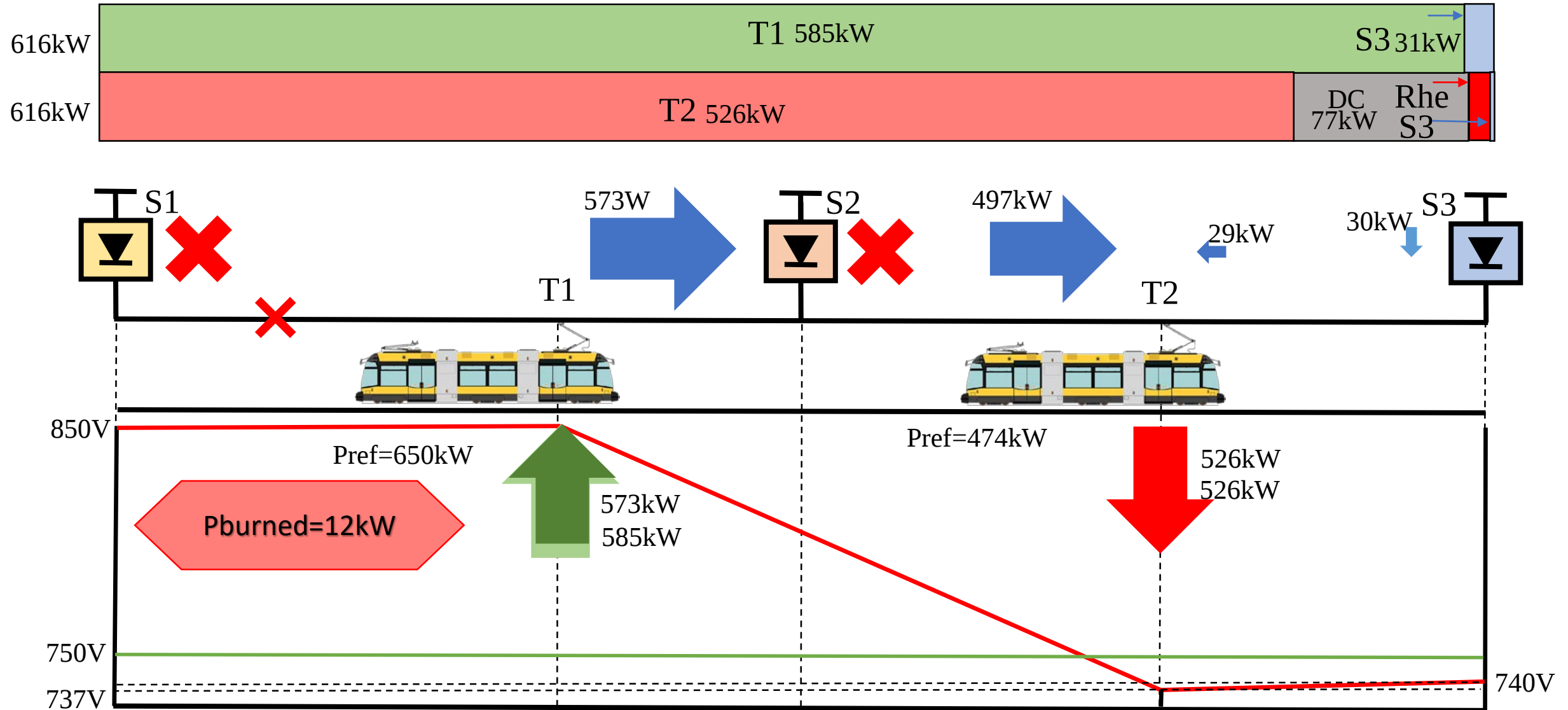
Conventional DC scenario (case 1)

Eff = 78%



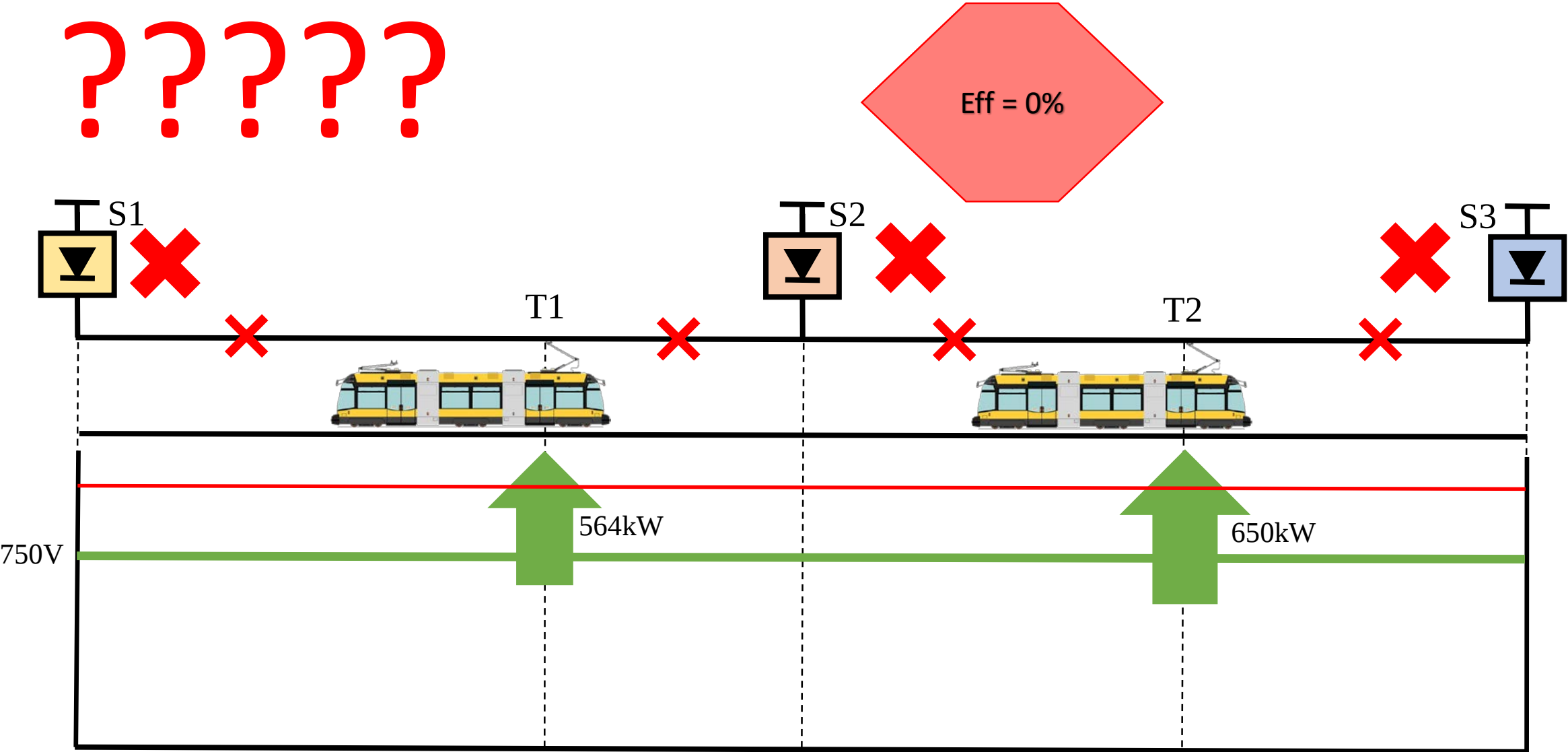
Conventional DC scenario (Case 2)

Eff = 85%



Conventional DC scenario

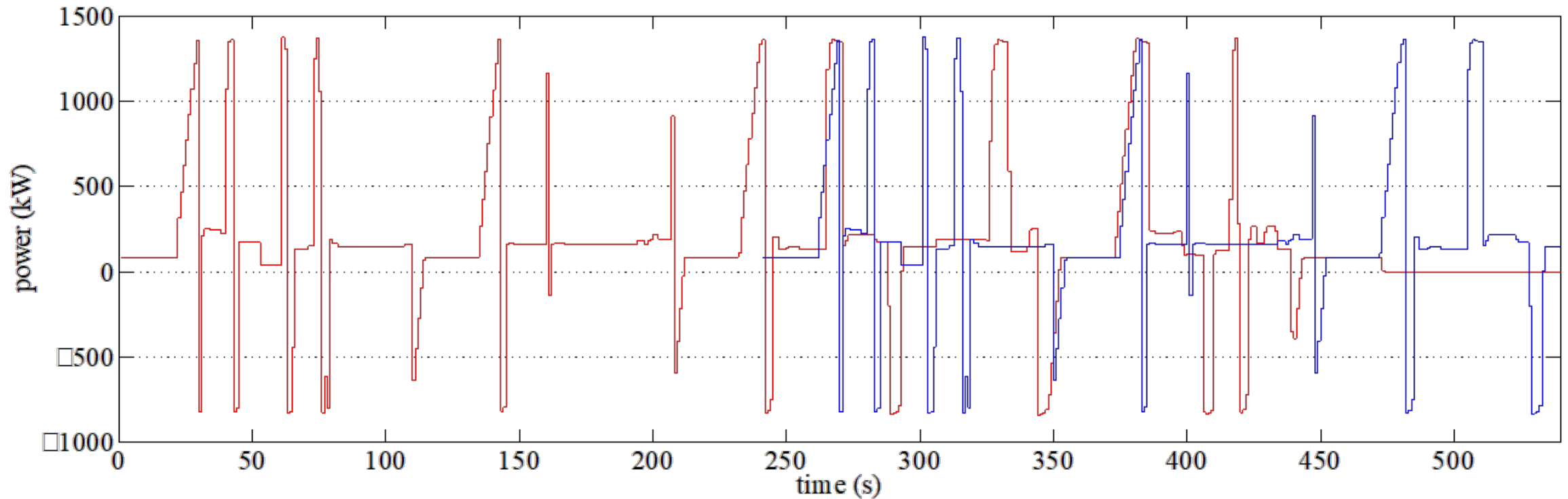
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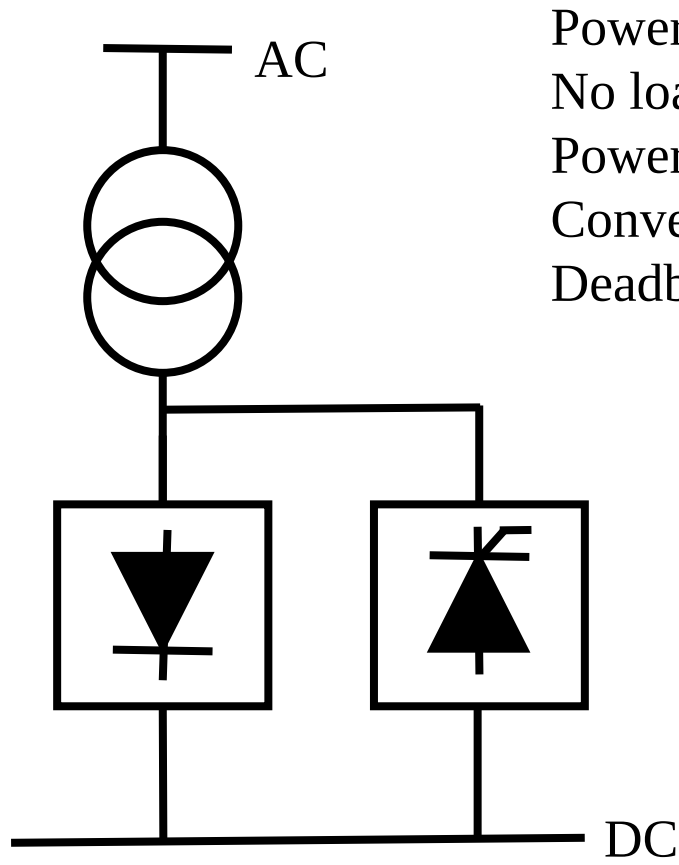
How often each scenario is present?

T2 - Blue

T1 - Red

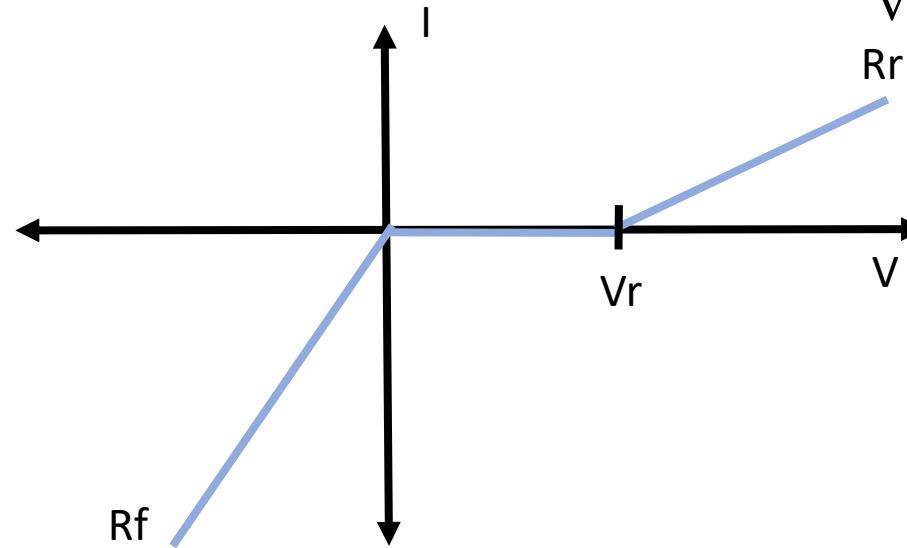


Reversible substations as a solution to increase the efficiency



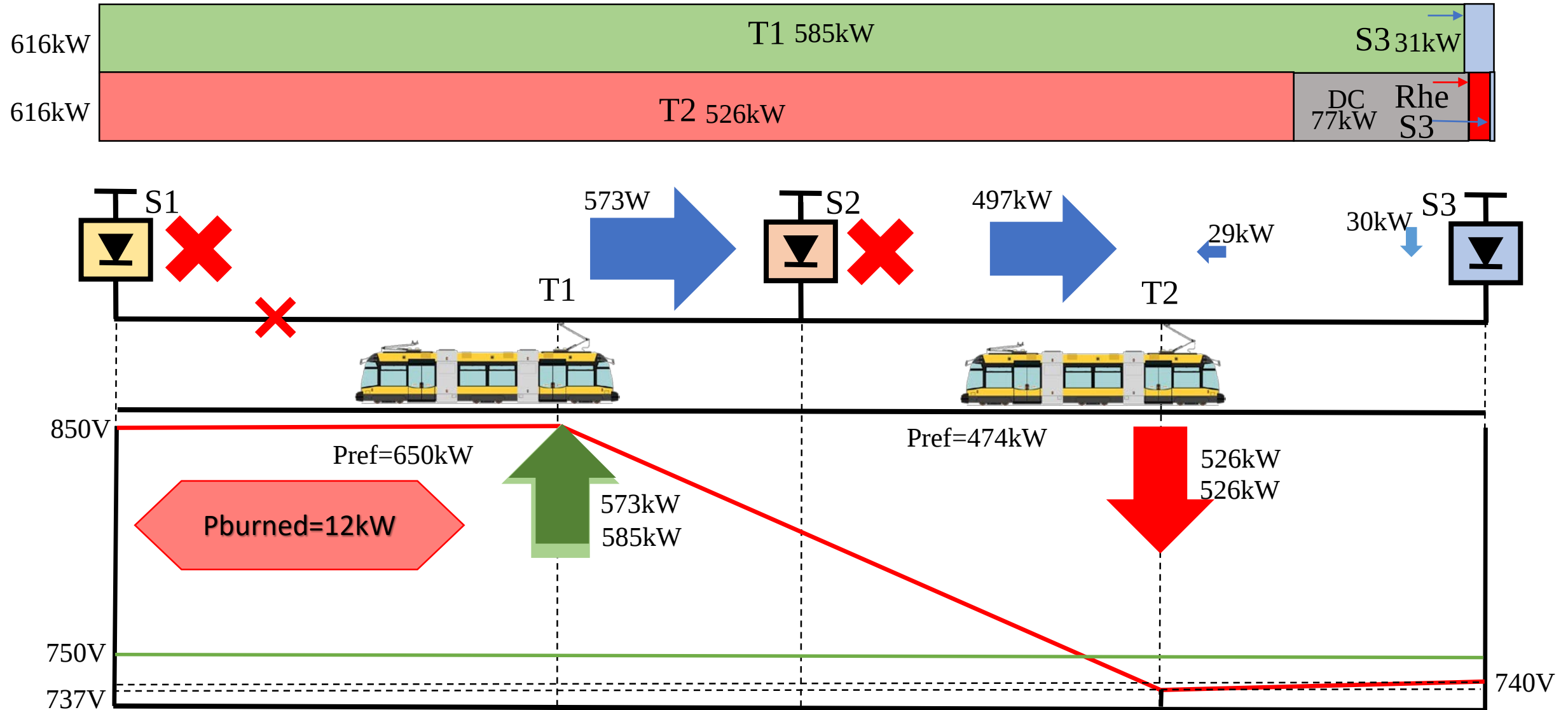
Power transformer and diode rectifier rated power:
No load and rated load DC voltage:
Power transformer s.c. voltage:
Converter rated power:
Deadband:

$P_r = 0,35 \text{ MW}$
 $V_0 = 750\text{V}, V_n = 700\text{V}$
 $V_{cc} = 8\%$
 $Pr = 0,175 \text{ MW}$
 $V_r = 10\text{V}$



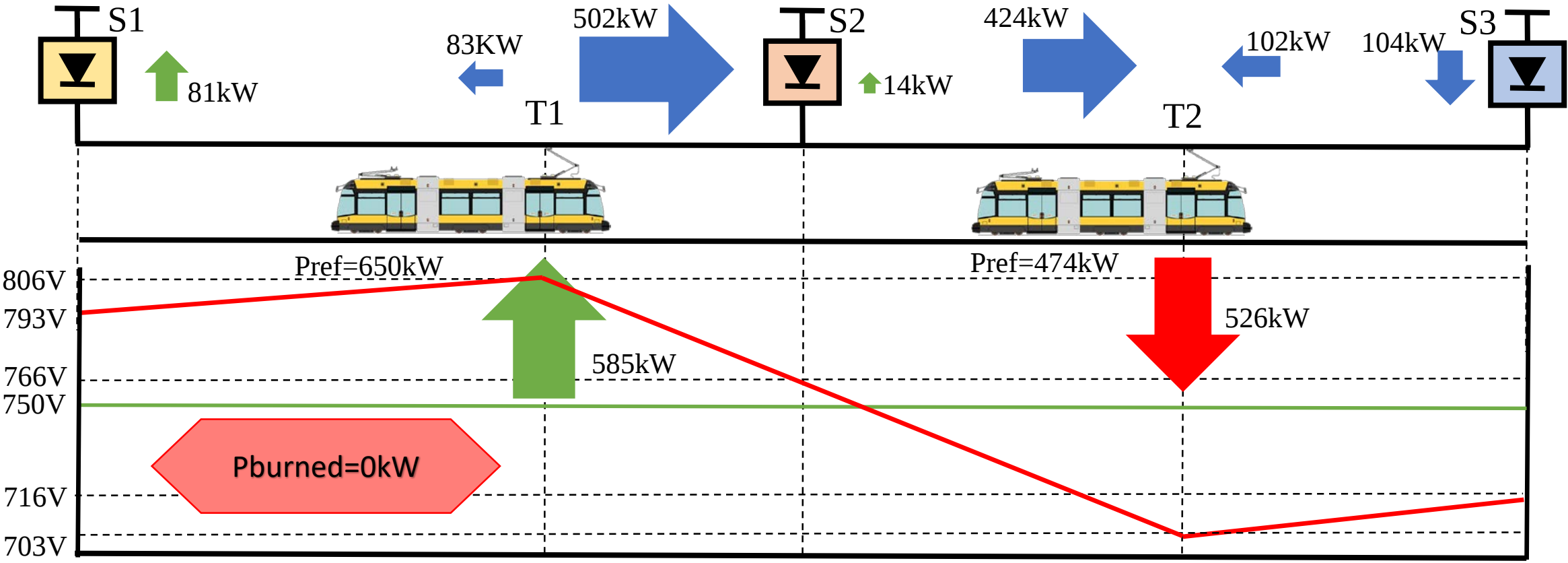
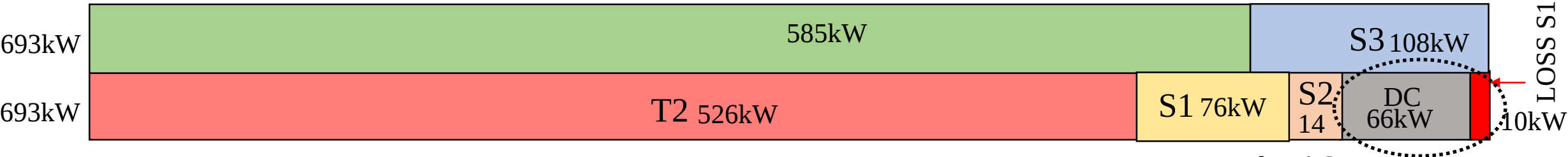
Conventional DC scenario (Case 2)

Eff = 85%

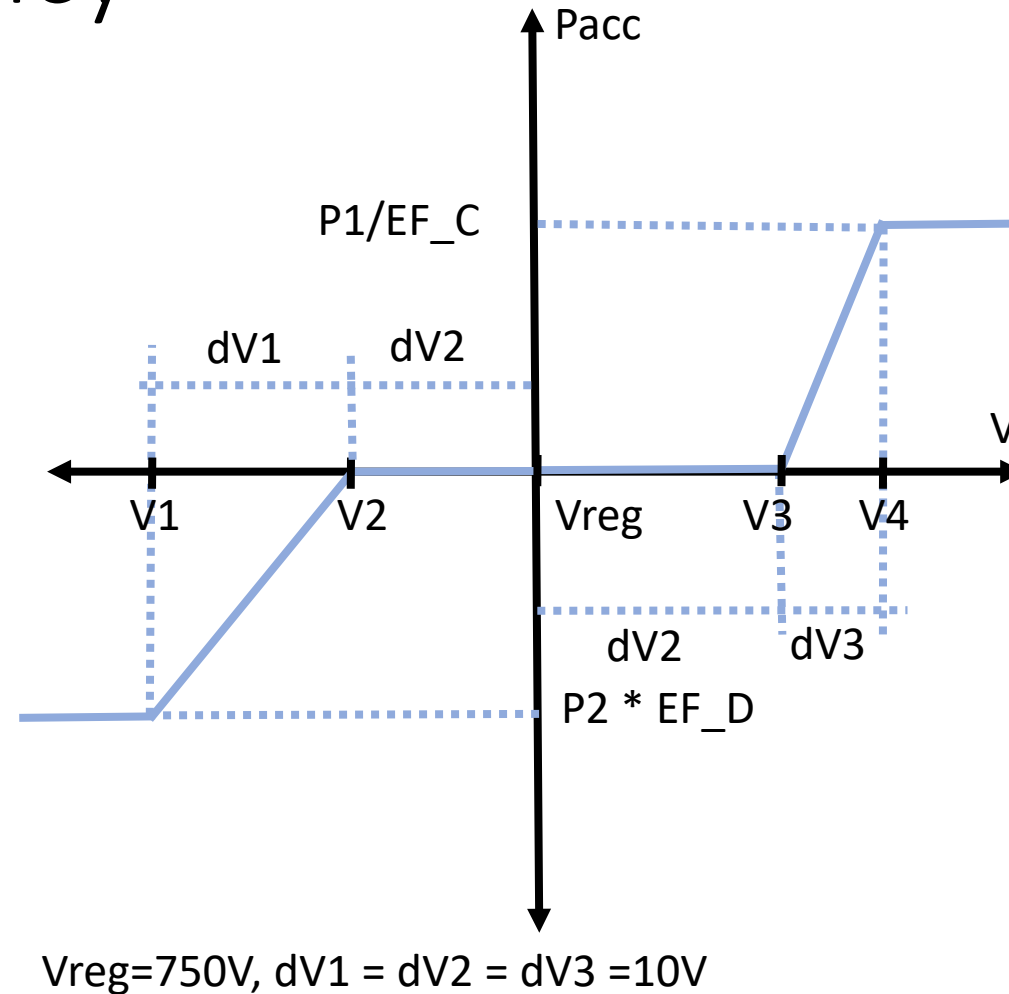
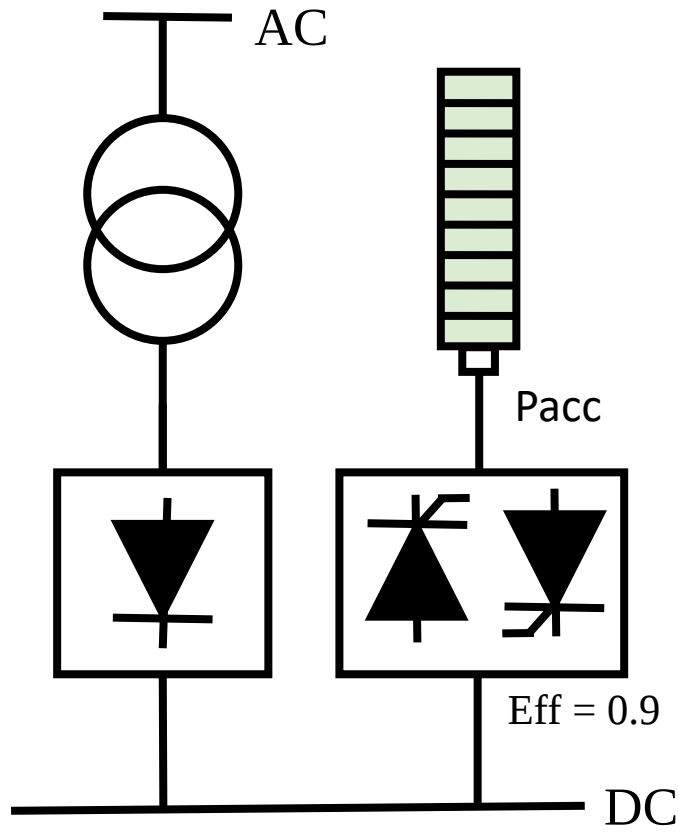


Reversible substations (Case 4)

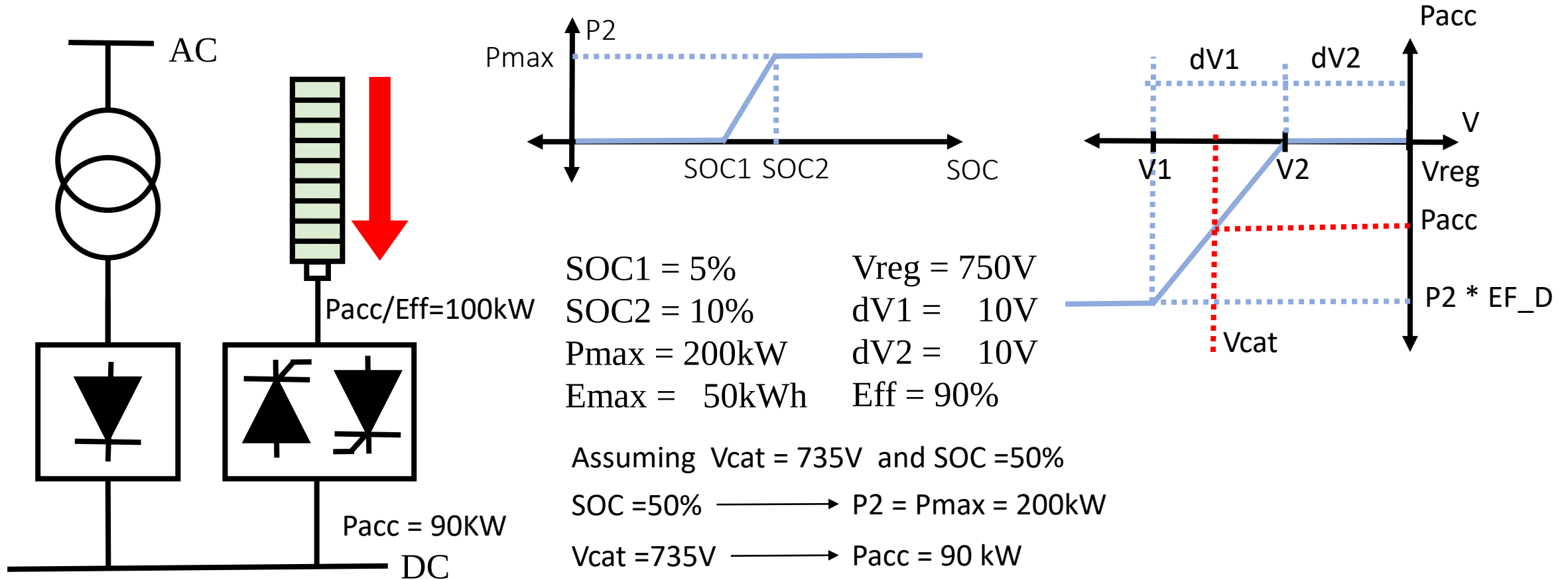
Eff = 90%



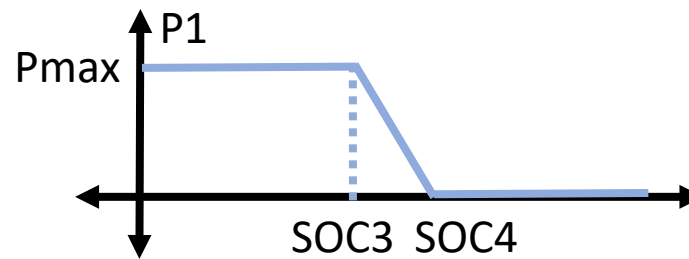
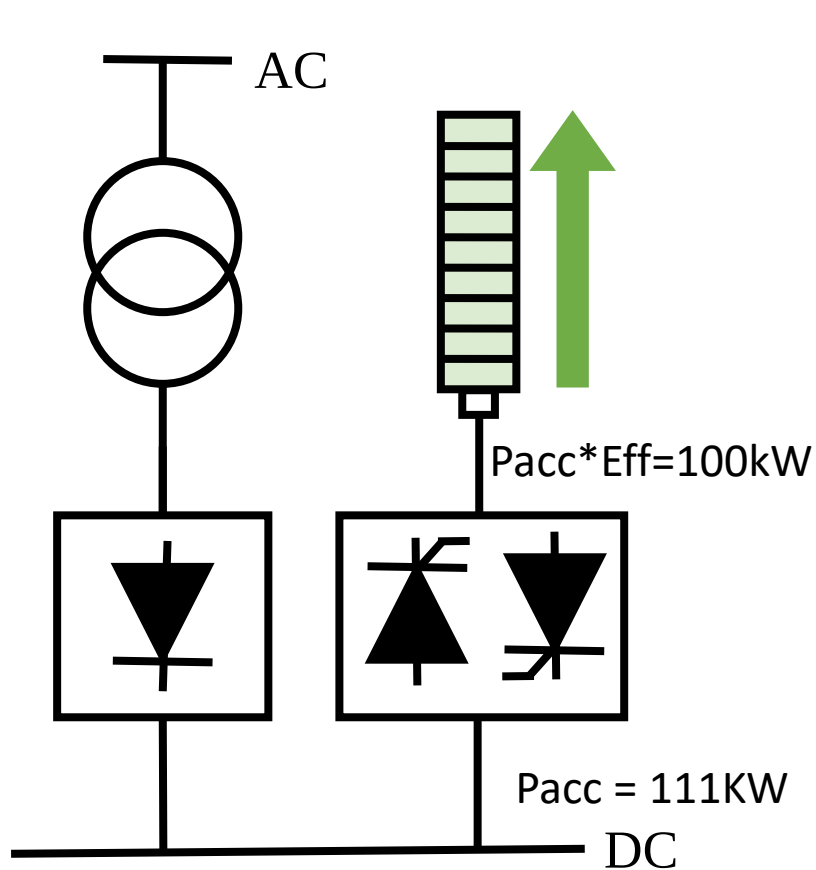
Off-board accumulation as a solution to increase the efficiency



Off-board accumulation as a solution to increase the efficiency (Discharging mode)



Off-board accumulation as a solution to increase the efficiency (Charging mode)

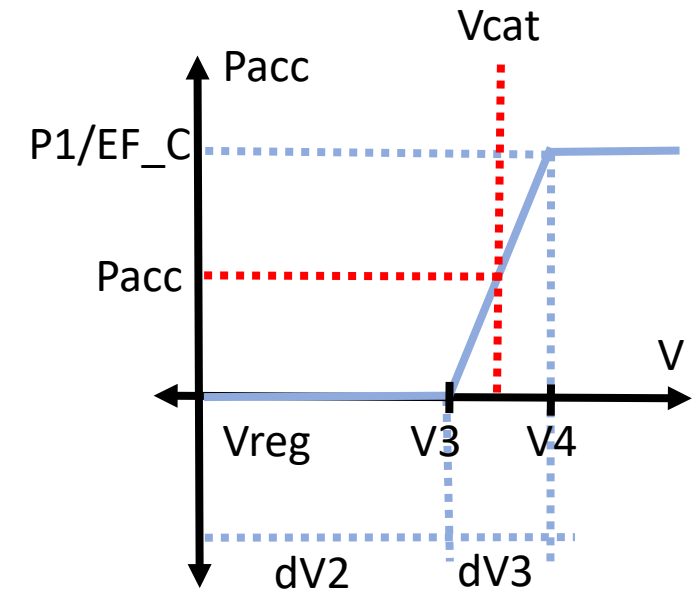


$SOC3 = 90\%$ $V_{reg} = 750V$
 $SOC4 = 95\%$ $dV2 = 10V$
 $P_{max} = 200kW$ $dV3 = 10V$
 $E_{max} = 50kWh$ $Eff = 90\%$

Assuming $V_{cat} = 765V$ and $SOC = 50\%$

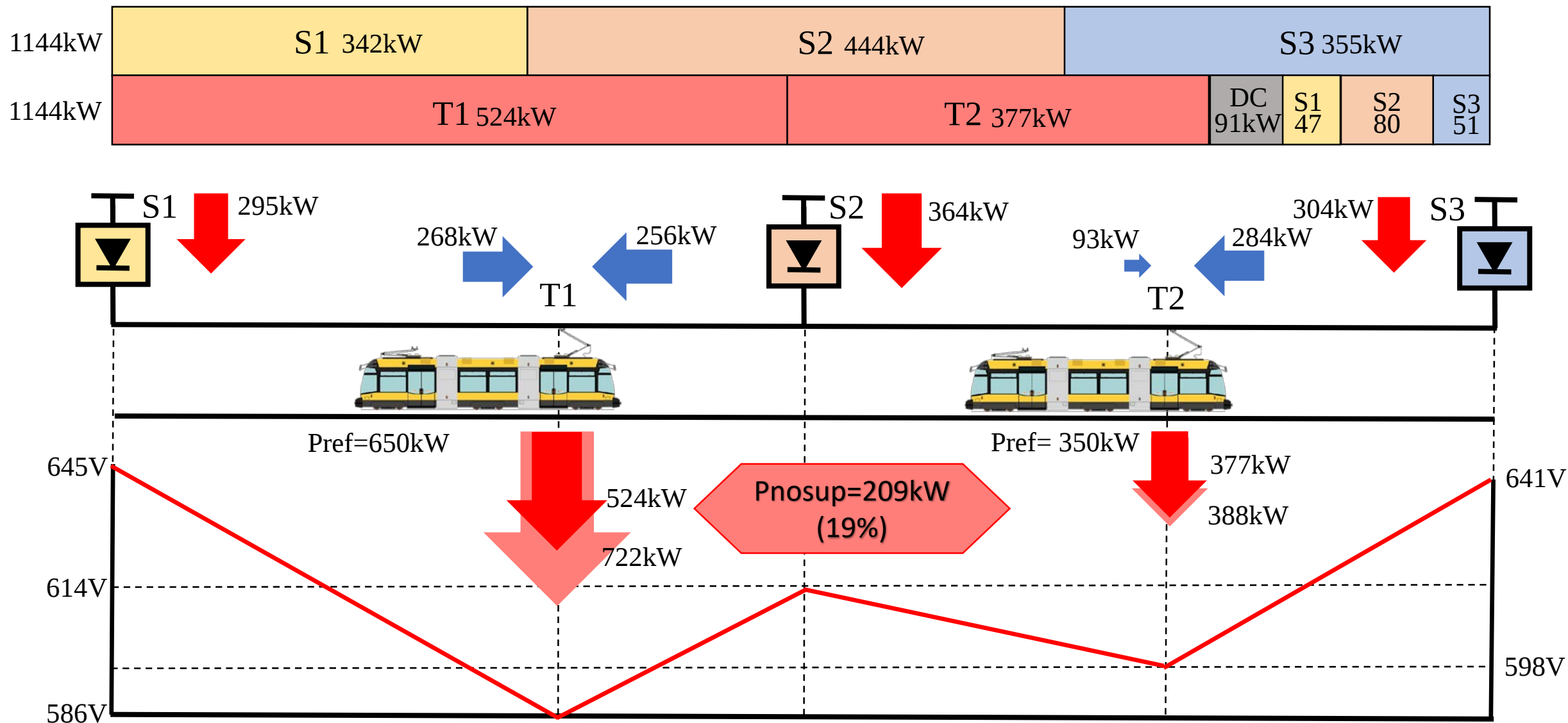
$SOC = 50\% \longrightarrow P1 = P_{max} = 200kW$

$V_{cat} = 765V \longrightarrow P_{acc} = 111 kW$



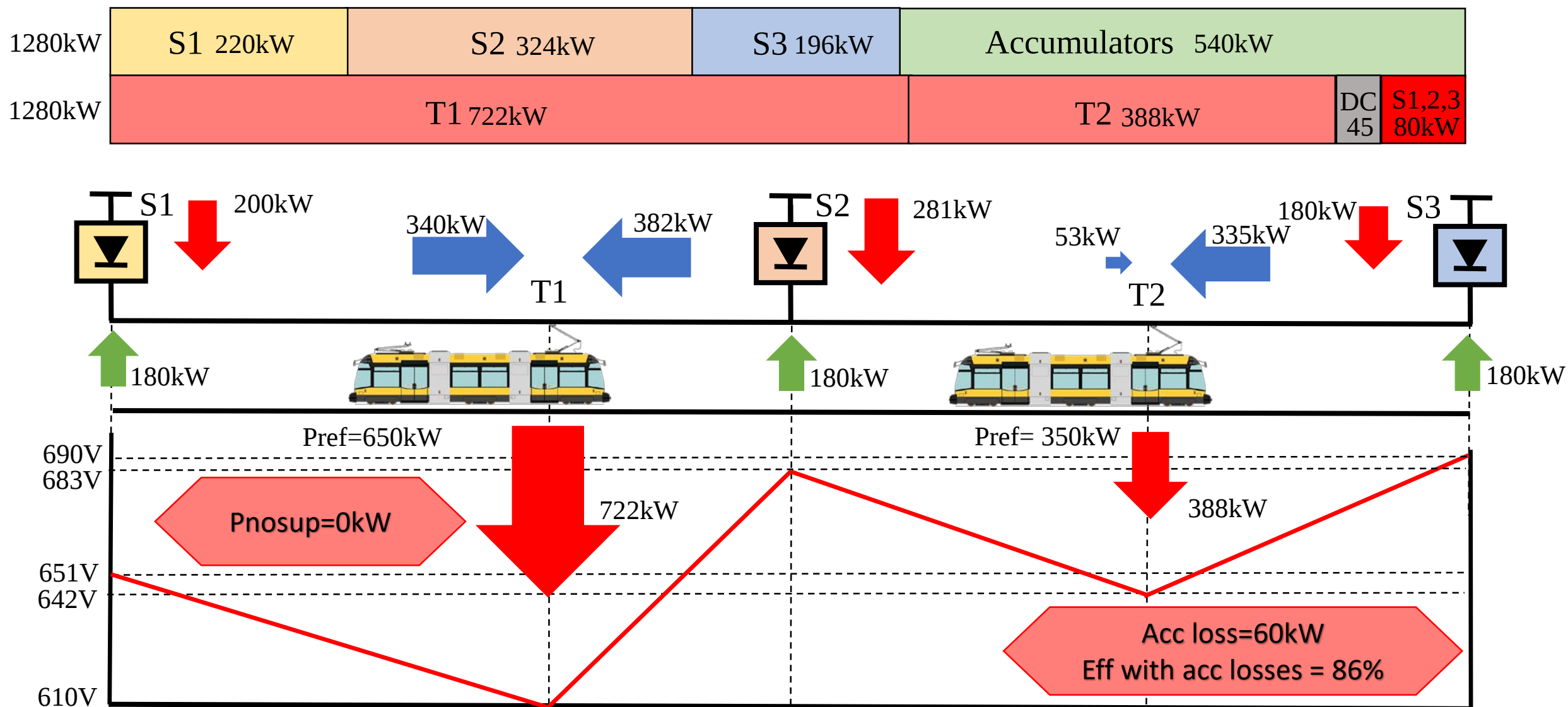
Conventional DC base scenario (case 1)

Eff = 78%

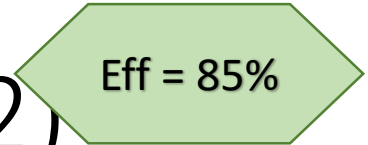


Off-board accumulation (case 5)

Eff = 90%

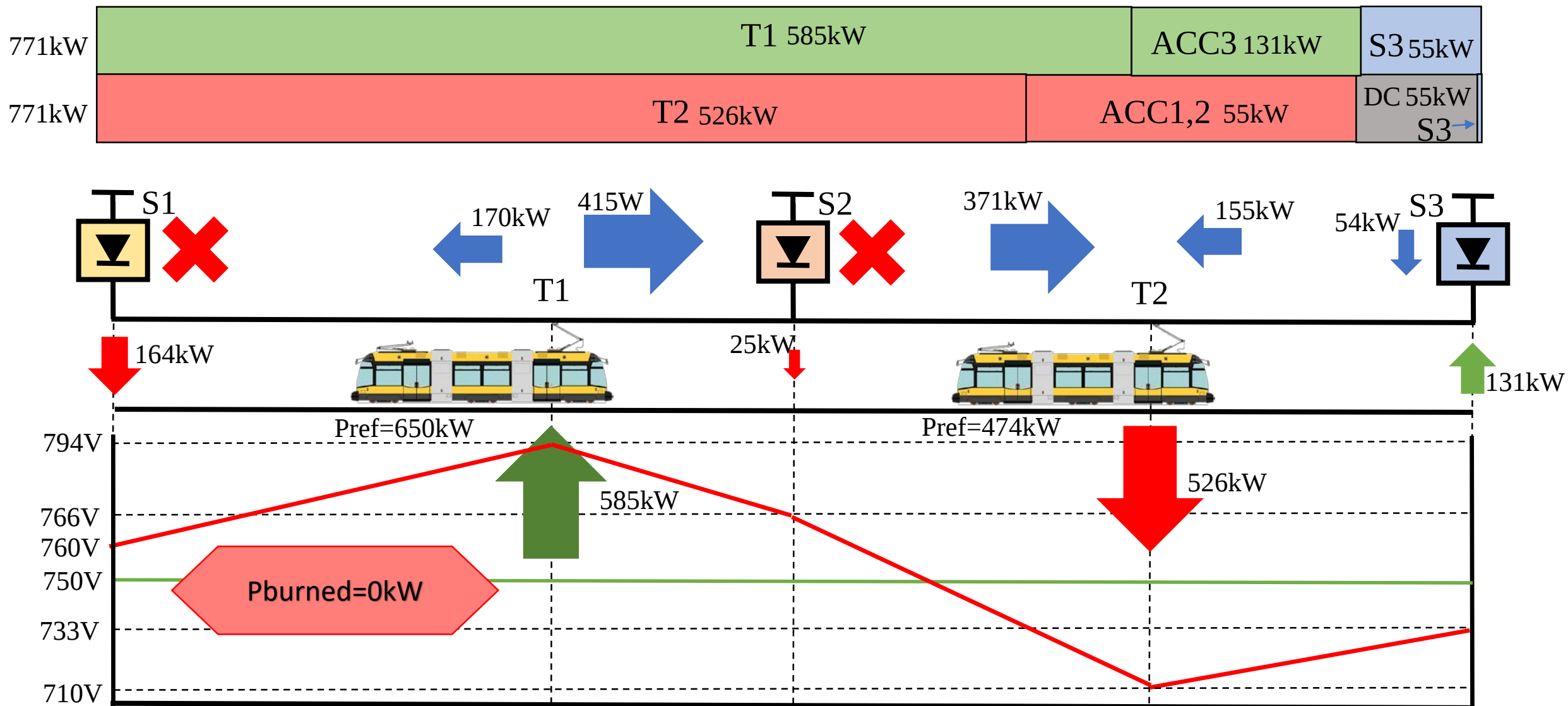


Eff = 85%



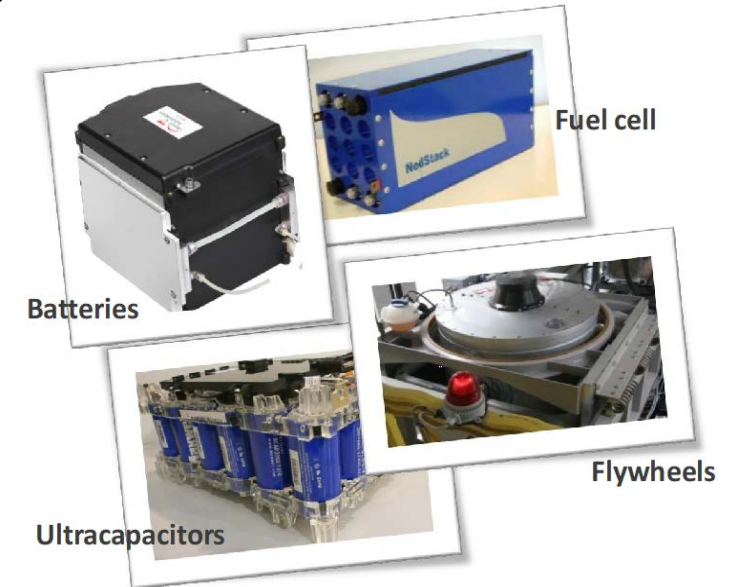
Off-board accumulation (Case 6)

Eff = 93%



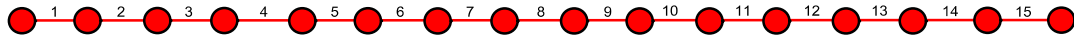
On board accumulation systems

Technologies/ Features							
	Life Cycle Cost	Energy Density	Power	Fast Charging	Availability	Safety	Maturity
Bad Medium Good							
Fuel-Cell (Hydr.)	Low	High	Med.	Yes	Med.	Low	Low
Batteries	Med.	High	Low	No	High	High	High
Flywheel	Med.	Low	High	Yes	Med.	Med.	High
Supercapacitors	Med.	Med.	High	Yes	High	High	High

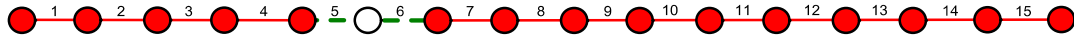


Hybridization of On-board accumulation systems

Evodrive



Low-Freedrive



Medium-Freedrive



High-Freedrive



- Catenary free section
- Catenary section
- Station non-energized
- Station energized

Ultracaps



Batteries

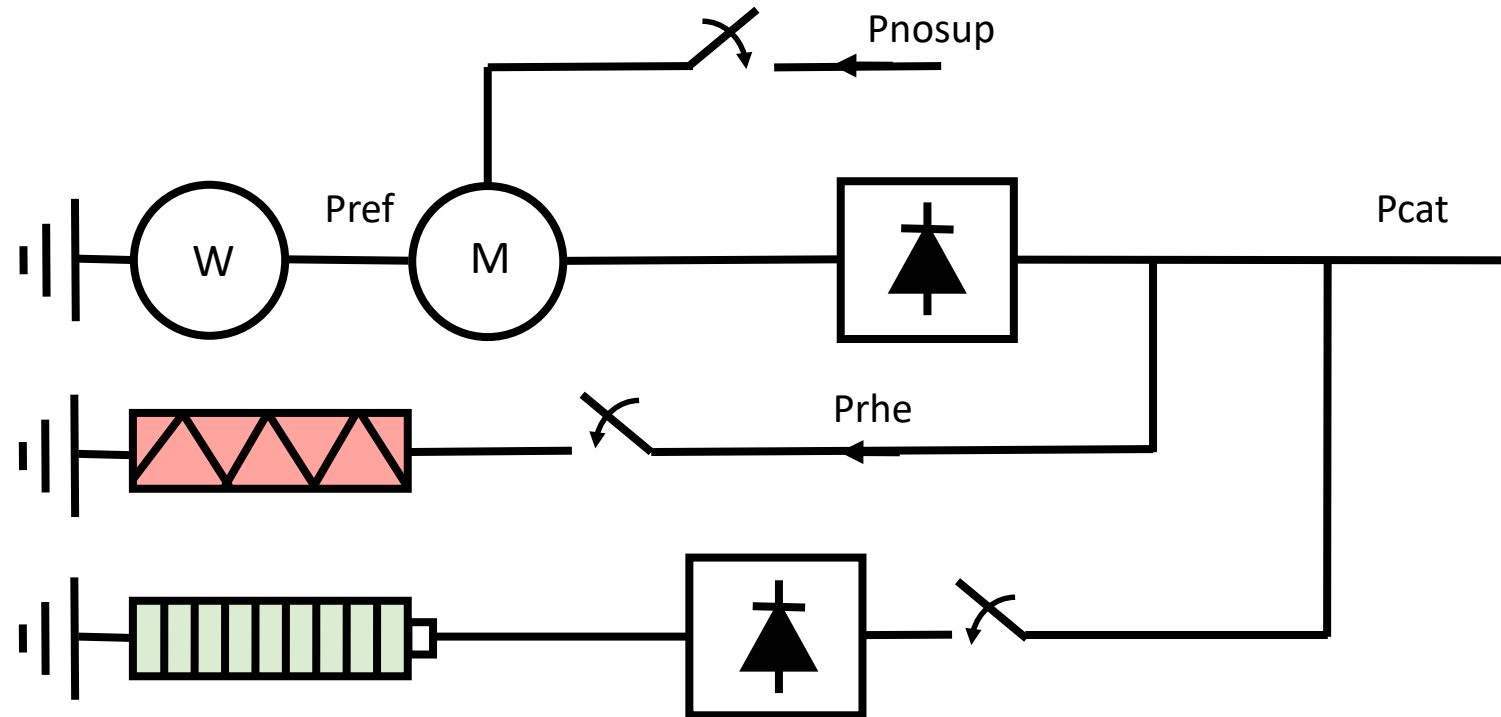


Charging stations

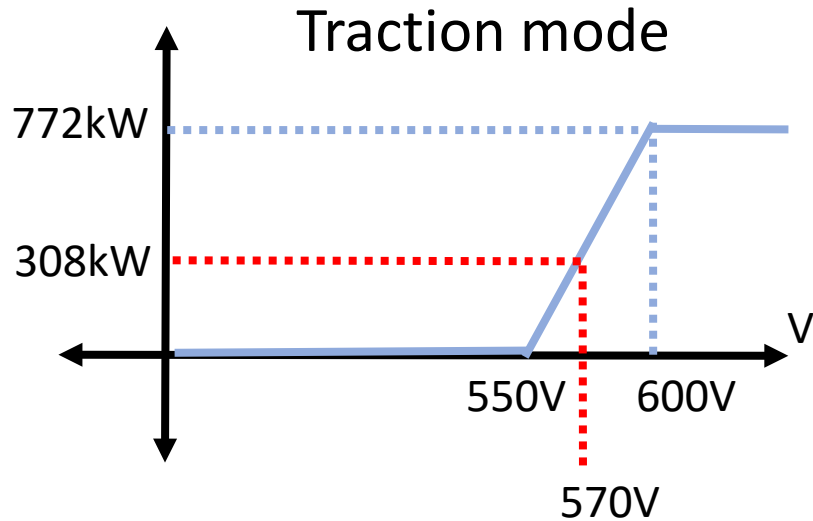


On-board accumulation as a solution to increase the efficiency

- The target at each instant is to make $P_{cat}=0$.
- The whole system will assign priority to the accumulation
- In traction mode, it will try to extract all demanded power from the accumulator, the rest will be extracted from the catenary (if possible).
- In braking mode, it will try to inject all the regenerated power into the accumulation system, the surplus will be injected in the network if possible, if not it will be burned in the rheostatic system.
- For calculation purposes the train and the storage system as considered as a separated devices as it will be shown in the next slides.

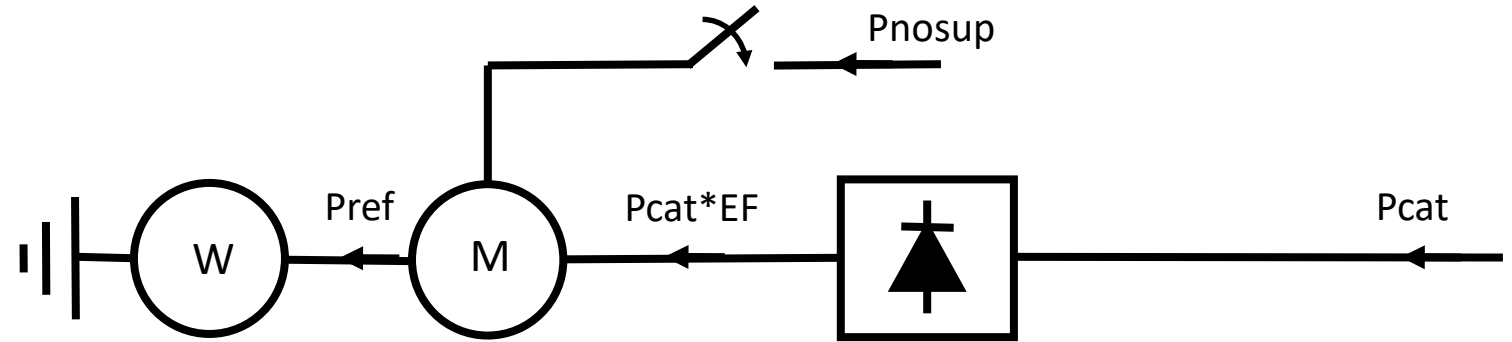
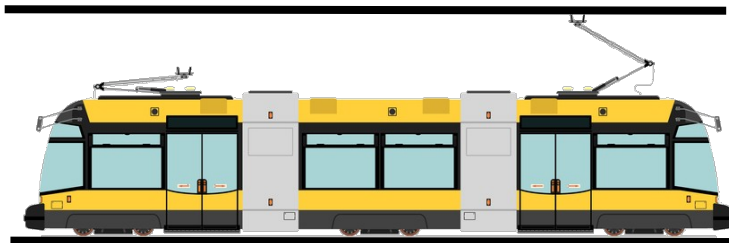


Train in traction mode – accumulator discharging



Efficiency = 0.9

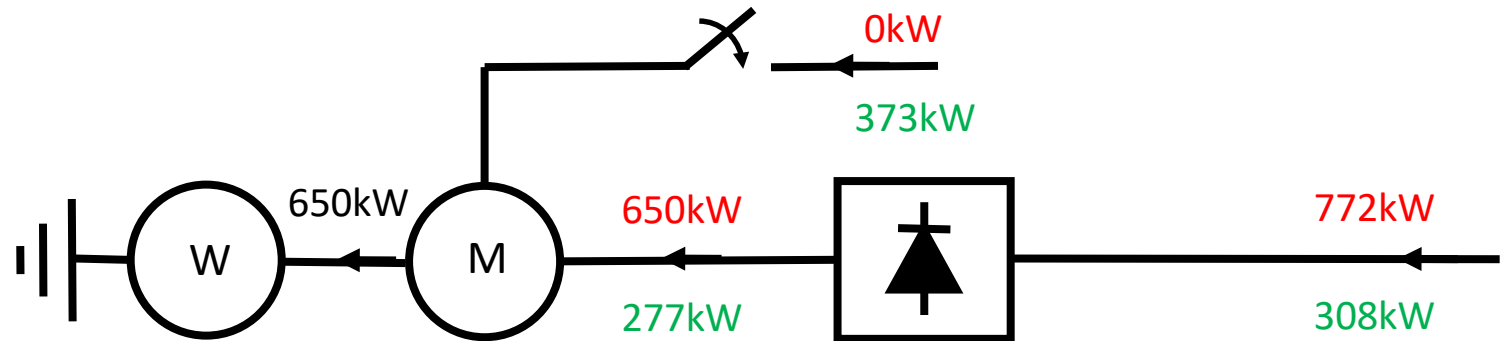
$V_1 = 550V$; $V_2 = 600V$



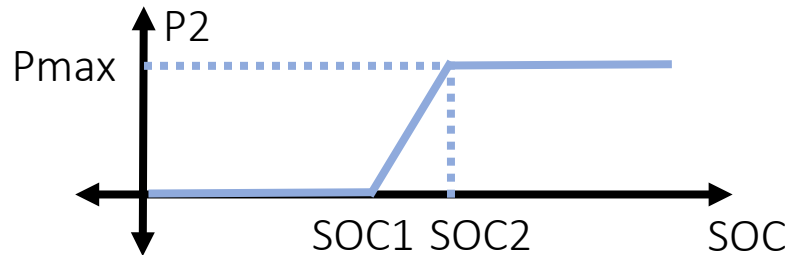
Assuming $V_{cat} = 570V$

$P_{ref} = 650kW$ → I need from the catenary $P_{ref}/EF = 722kW$

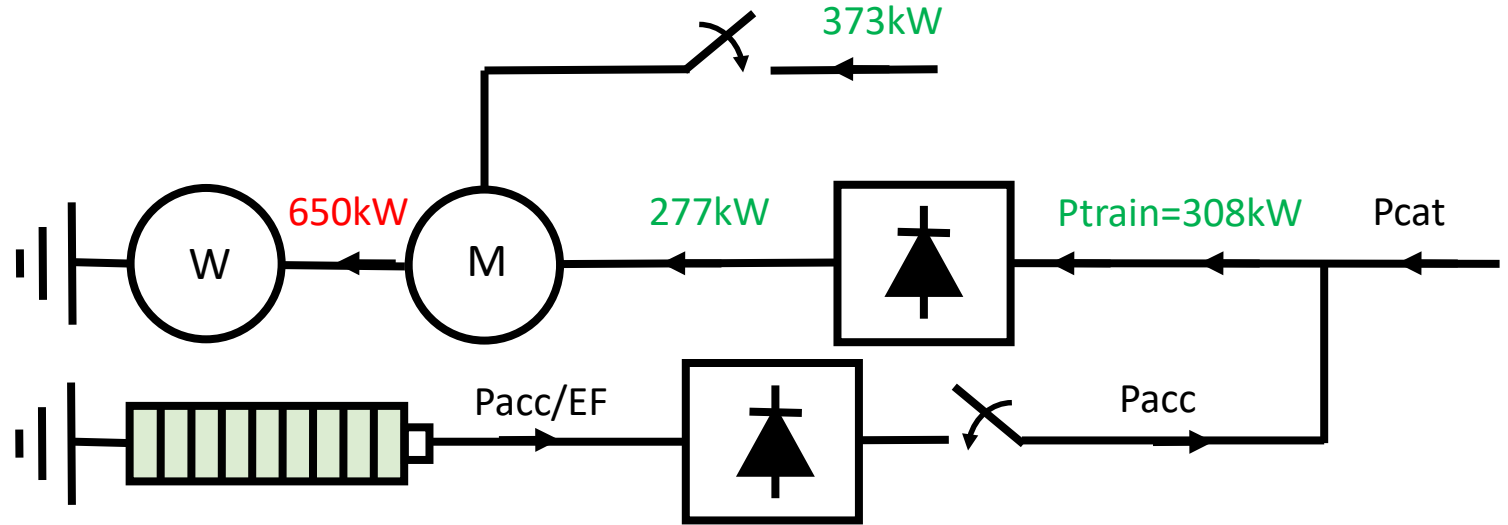
The overcurrent protection limits the power to 308kW



Train in traction mode – accumulator discharging



$SOC1 = 5\%$
 $SOC2 = 10\%$
 $P_{max} = 300kW$
 $E_{max} = 20kWh$
 $Eff = 90\%$

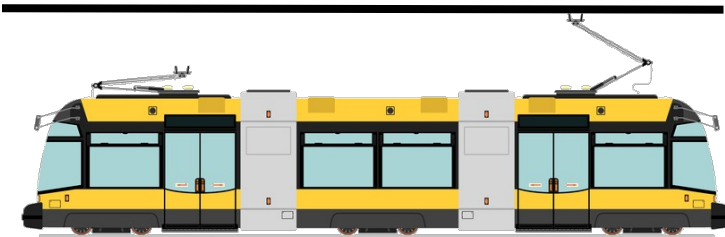


Assuming $V_{cat} = 570V$ and $SOC = 50\%$

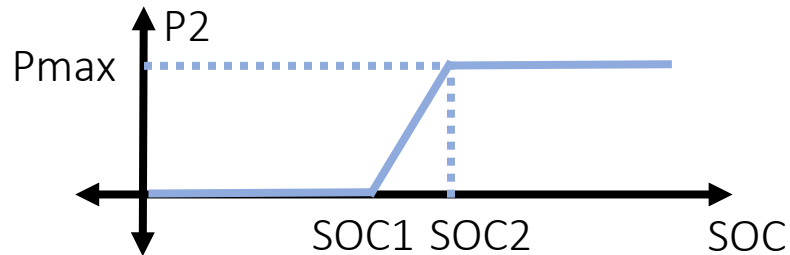
$SOC = 50\% \longrightarrow P_2 = P_{max} = 300kW \longrightarrow P_{acc_available} = P_{max} * Eff = 270kW$

$P_{acc} = \min(P_{acc_available}, P_{train}) = \min(270, 308) = 270kW$

$P_{cat} = P_{train} - P_{acc} = 308 - 270 = 38kW$



Train in traction mode – accumulator discharging



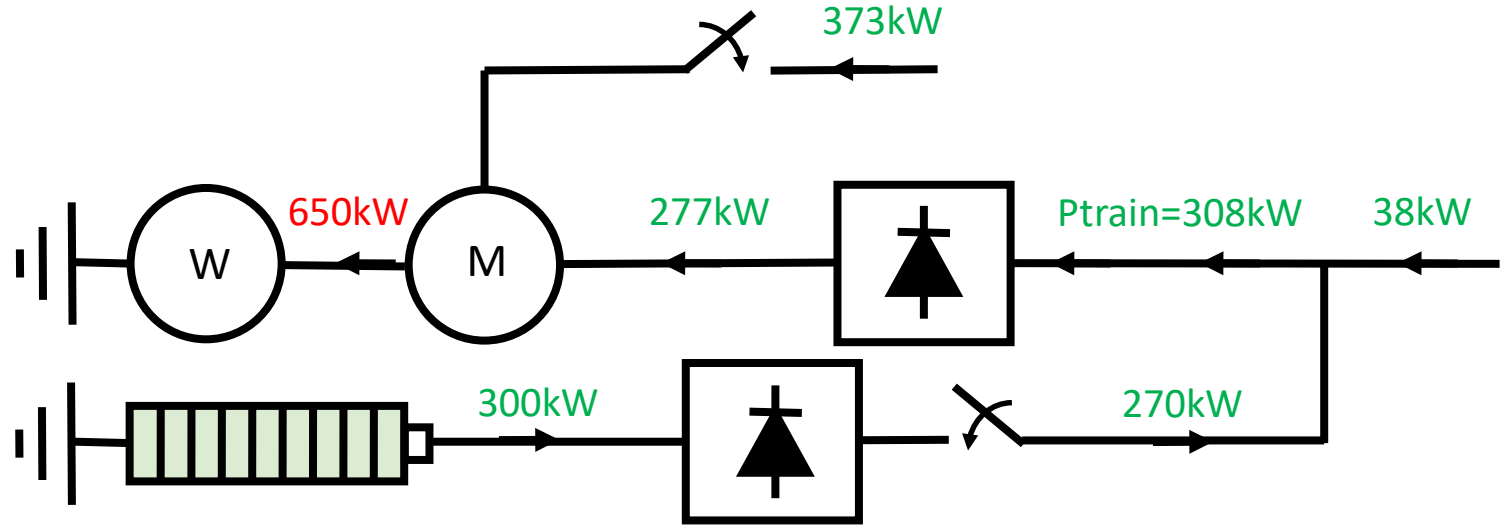
SOC1 = 5%

SOC2 = 10%

$P_{max} = 300\text{kW}$

$E_{max} = 20\text{kWh}$

Eff = 90%

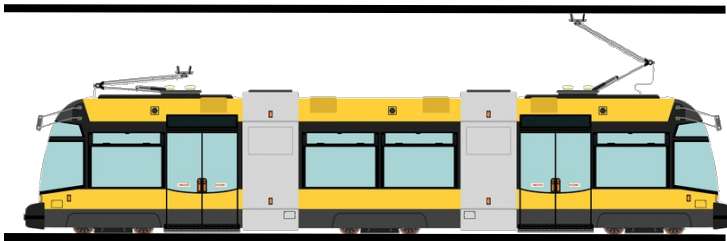


Assuming $V_{cat} = 570\text{V}$ and SOC = 50%

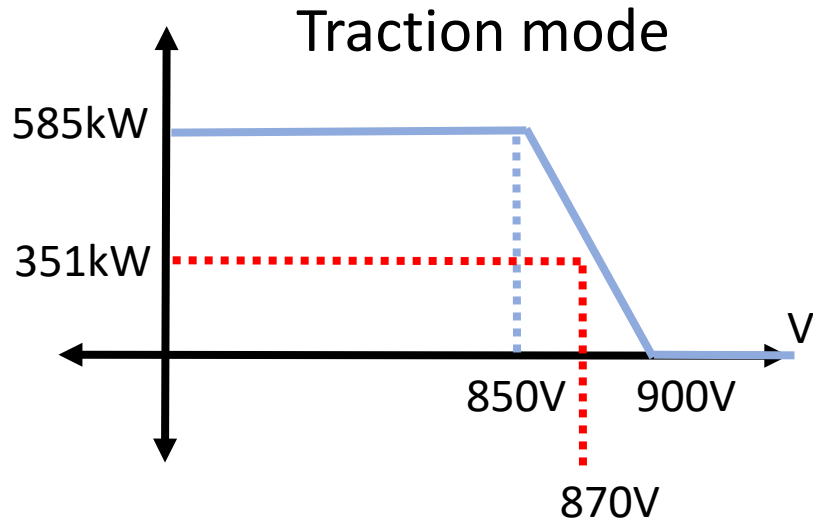
SOC = 50% $\longrightarrow$ $P_2 = P_{max} = 300\text{kW}$ $\longrightarrow$ $P_{acc_available} = P_{max} \cdot \text{Eff} = 270\text{kW}$

$P_{acc} = \min(P_{acc_available}, P_{train}) = \min(270, 308) = 270\text{kW}$

$P_{cat} = P_{train} - P_{acc} = 308 - 270 = 38\text{kW}$

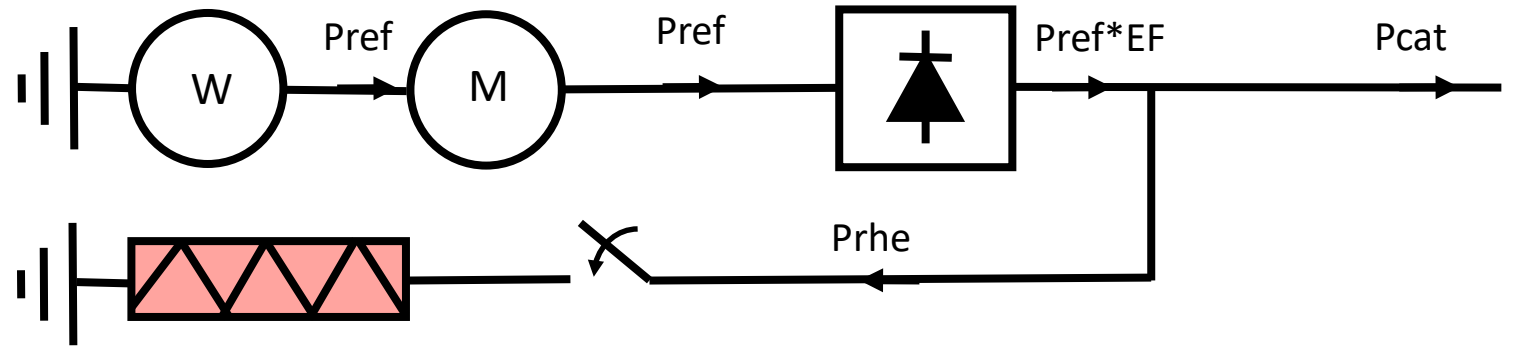
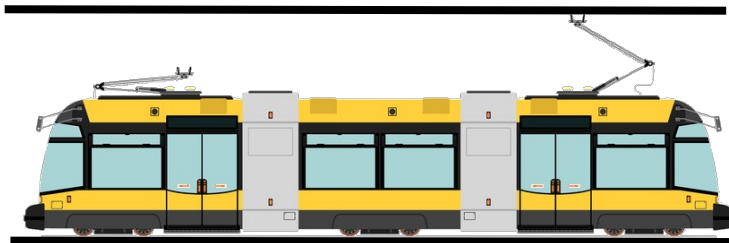


Train in braking mode – accumulator charging



Efficiency = 0.9

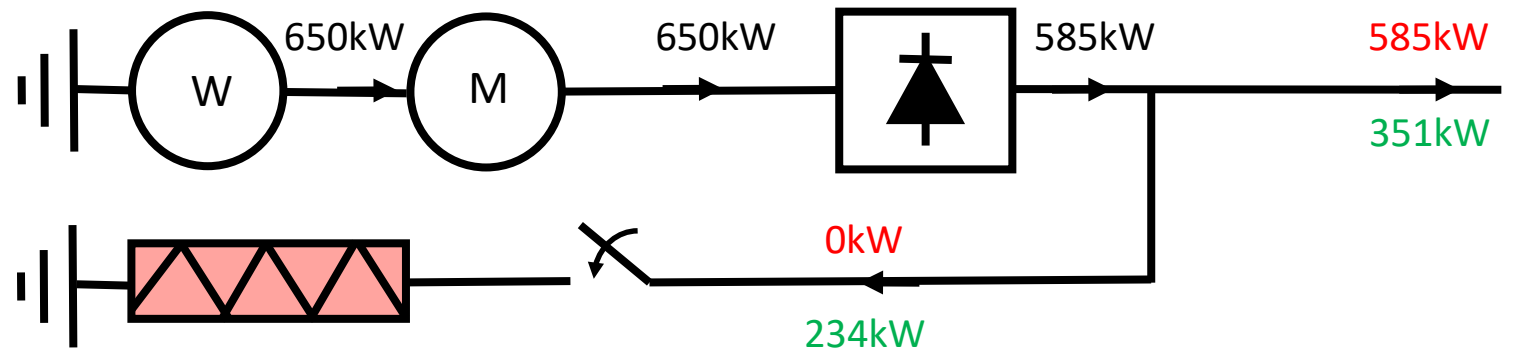
$V_3 = 850V$; $V_4 = 900V$



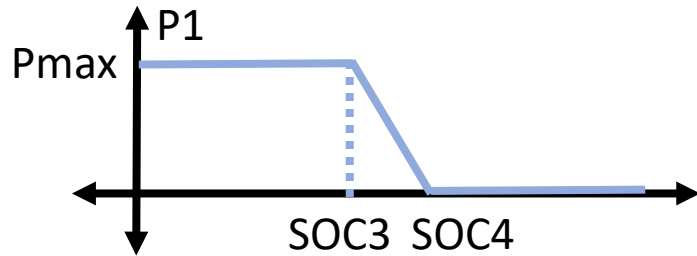
Assuming $V_{cat} = 870V$

$P_{ref} = 650kW \longrightarrow$ I would like to inject in the catenary $P_{ref} * EF = 585kW$

The overvoltage protection limits the power to 351kW



Train in braking mode – accumulator charging



SOC1 = 90%

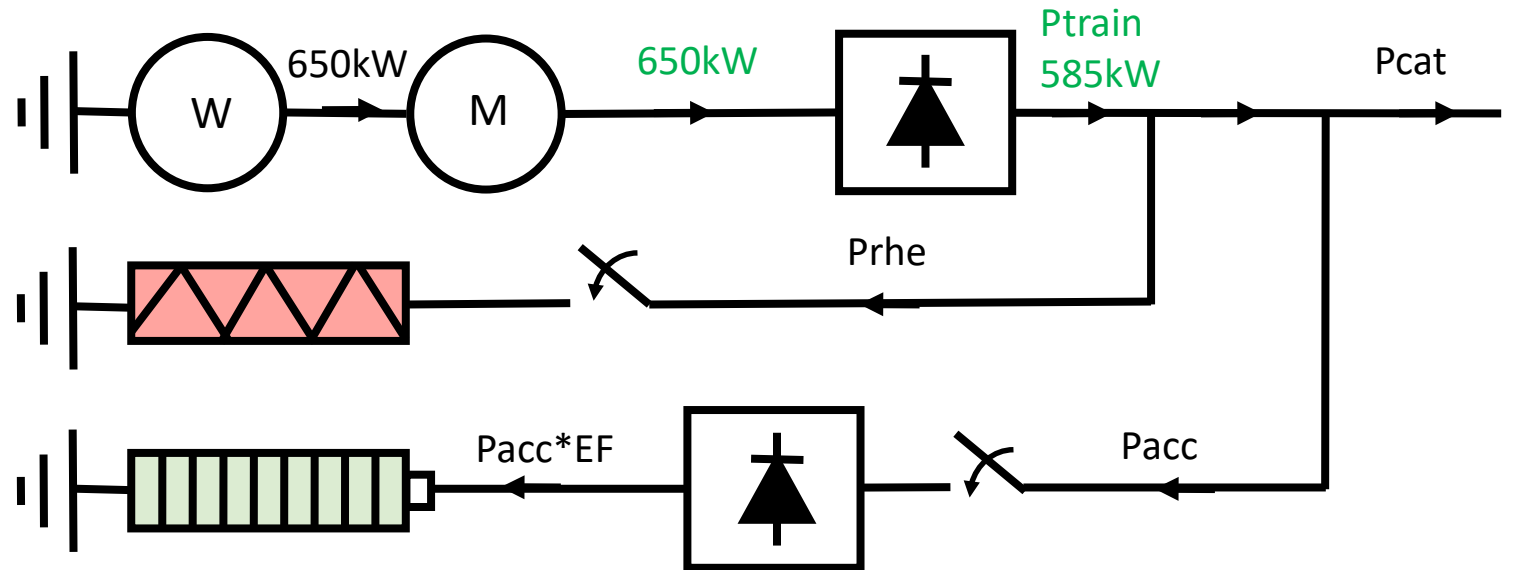
SOC2 = 95%

$P_{max} = 300\text{kW}$

$E_{max} = 20\text{kWh}$

$Eff = 90\%$

$P_{cat_max} = 351\text{kW}$



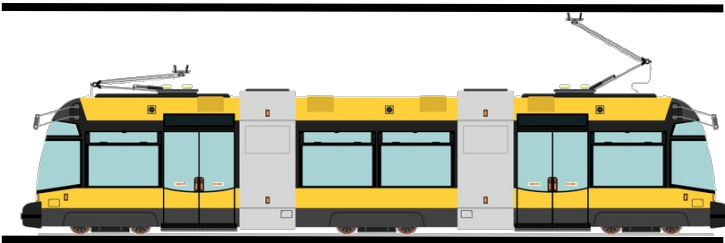
Assuming $V_{cat} = 870\text{V}$ and $SOC = 50\%$

$SOC = 50\% \longrightarrow P_1 = P_{max} = 300\text{kW} \longrightarrow P_{acc_available} = P_{max}/Eff = 333\text{kW}$

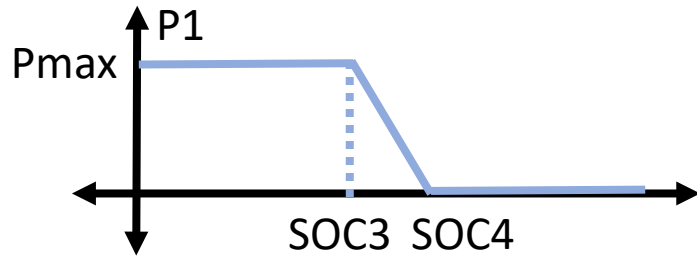
$P_{acc} = \min(P_{acc_available}, P_{train}) = \min(333, 585) = 333\text{kW}$

$P_{cat} = \min(P_{train} - P_{acc}, P_{cat_max}) = \min(252, 351) = 252\text{kW}$

$P_{rhe} = P_{train} - P_{acc} - P_{cat} = 585 - 333 - 252 = 0\text{kW}$



Train in braking mode – accumulator charging



SOC1 = 90%

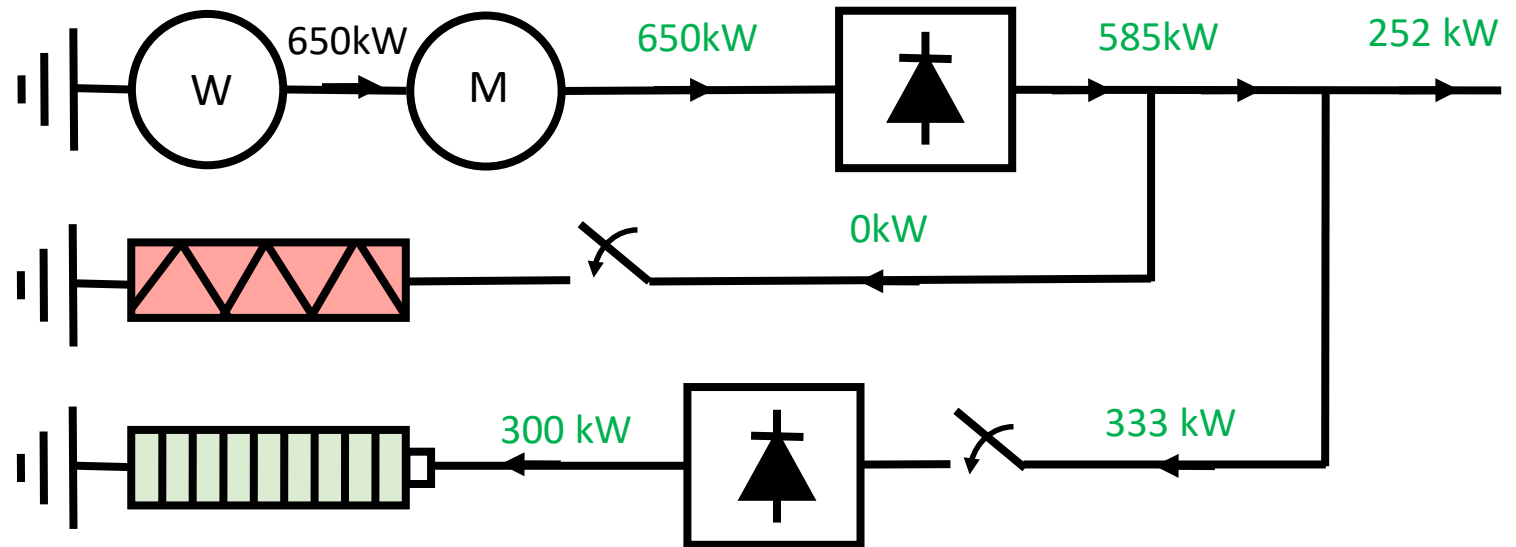
SOC2 = 95%

$P_{max} = 300\text{kW}$

$E_{max} = 20\text{kWh}$

$\text{Eff} = 90\%$

$P_{cat_max} = 351\text{kW}$



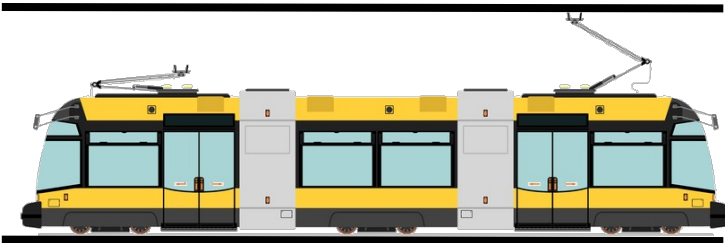
Assuming $V_{cat} = 870\text{V}$ and $\text{SOC} = 50\%$

$\text{SOC} = 50\% \longrightarrow P1 = P_{max} = 300\text{kW} \longrightarrow P_{acc_available} = P_{max}/\text{Eff} = 333\text{kW}$

$P_{acc} = \min(P_{acc_available}, P_{train}) = \min(585, 333) = 333\text{kW}$

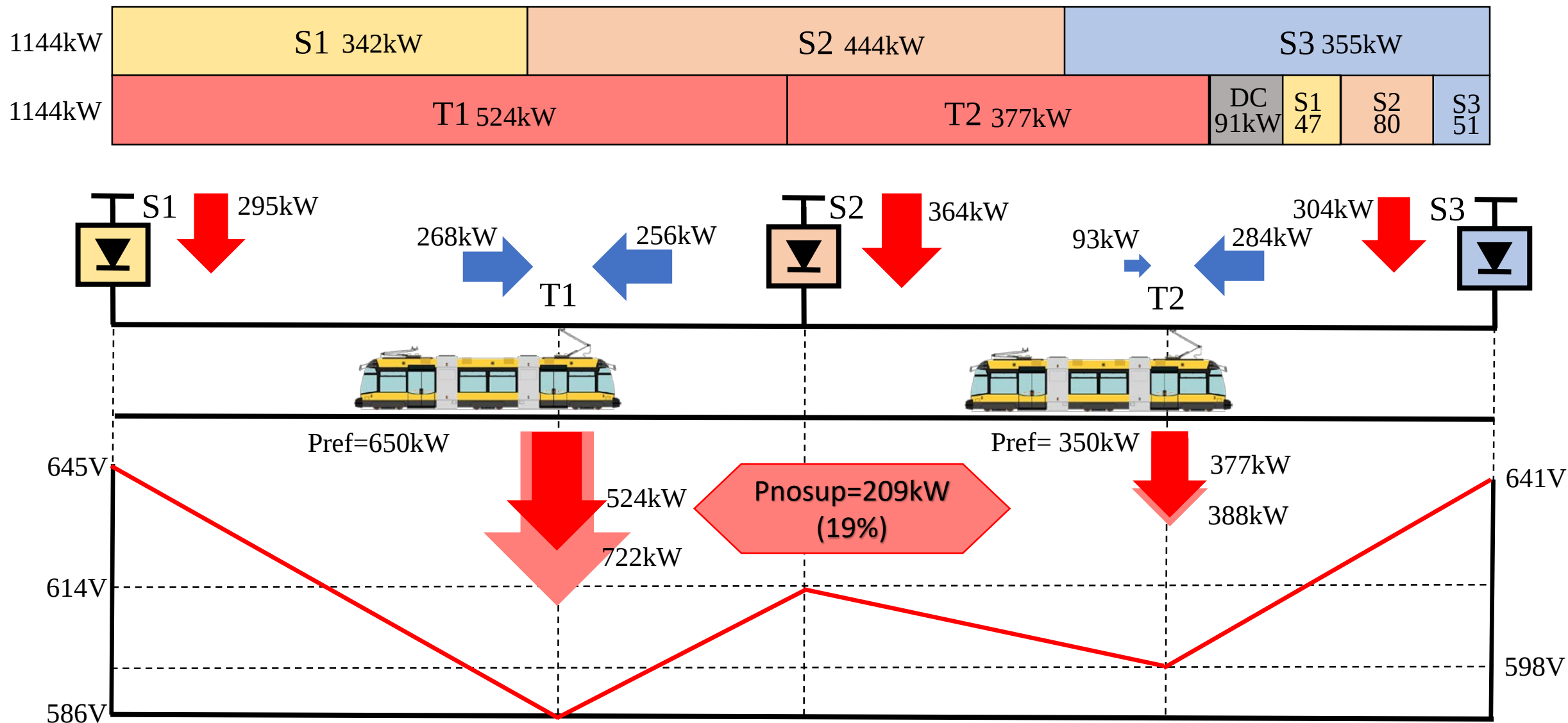
$P_{cat} = \min(P_{train} - P_{acc}, P_{cat}) = \min(252, 351) = 252\text{kW}$

$P_{rhe} = P_{train} - P_{acc} - P_{cat} = 585 - 333 - 252 = 0\text{kW}$



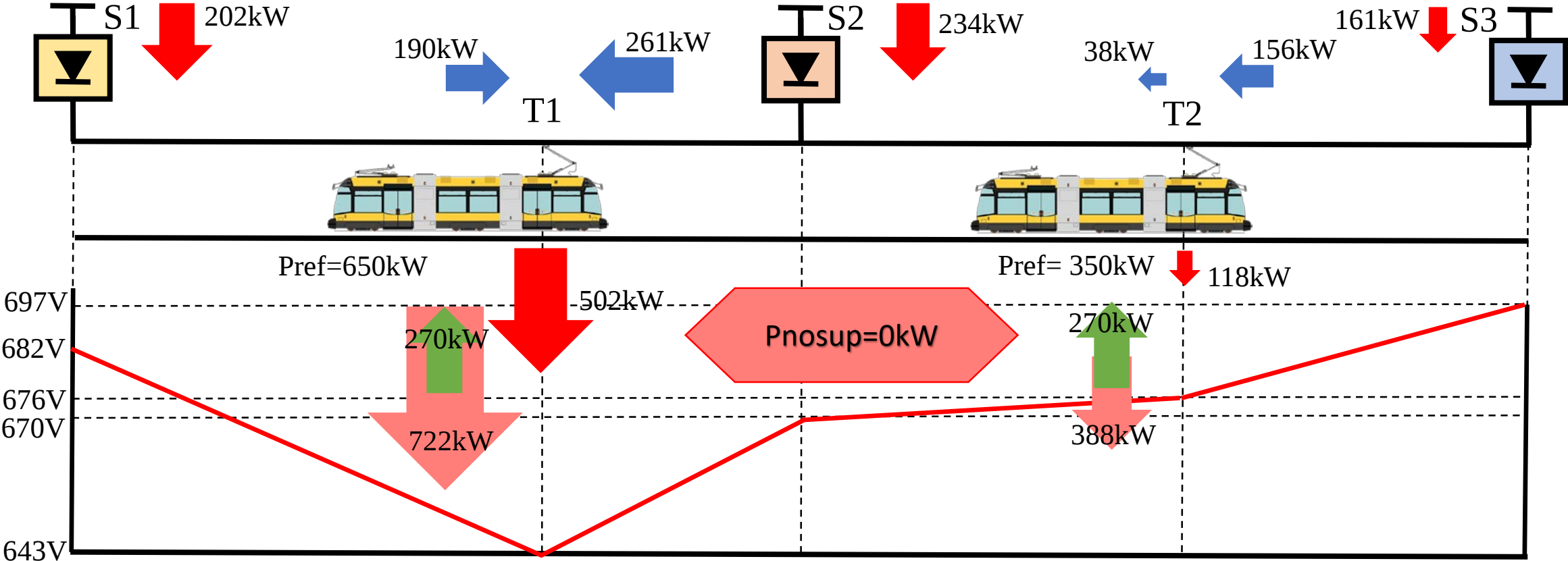
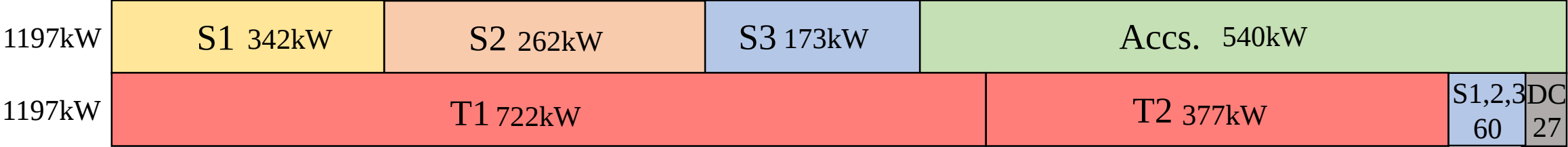
Conventional DC base scenario (case 1)

Eff = 78%



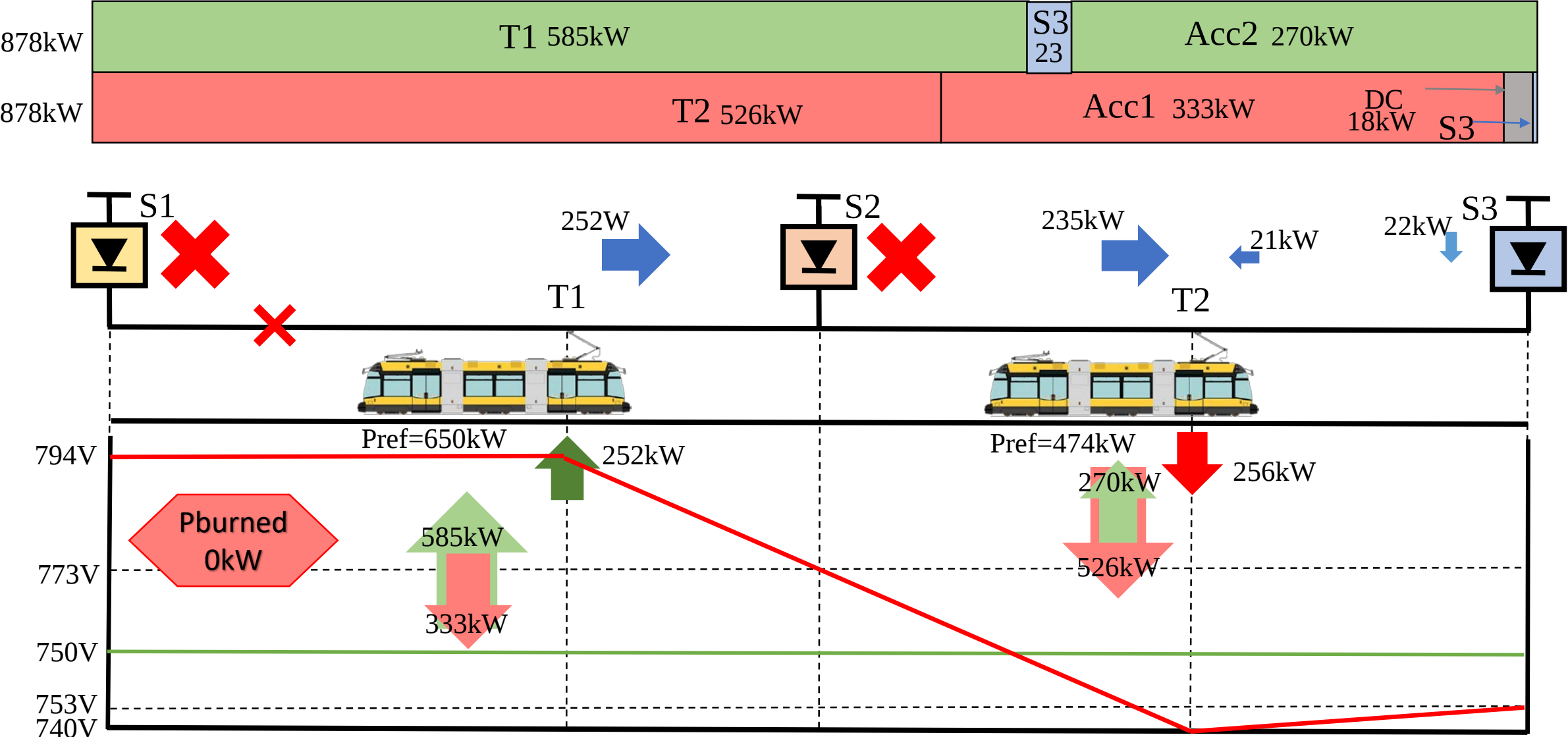
Eff = 93%

On-board accumulation (case 7)



Eff = 98%

On-board accumulation (Case 8)



Cases of study (Summary)

	Substations ****	Trains Acc. ***	Train controls **	Pref T1 *	Pref T2 *	Total P(kW)	P burned (kW)	P non-sup. (kW)	Efficiency (%)
Case 1	Non-reversible	No	Yes	650	350	1144	0	209	78
Case 2	Non-reversible	No	Yes	-650	474	616	12	0	85
Case 3	Reversible	No	Yes	650	350	1144	0	0	78
Case 4	Reversible	No	Yes	-650	474	693	0	0	90
Case 5	Non-rev + Acc	No	Yes	650	350	1280	0	0	90
Case 6	Non-rev + Acc	No	Yes	-650	474	771	0	0	93
Case 7	Non-reversible	Yes	Yes	650	350	1197	0	0	93
Case 8	Non-reversible	Yes	Yes	-650	474	878	0	0	98

* Negative reference power in the trains means that the train is braking and regenerating

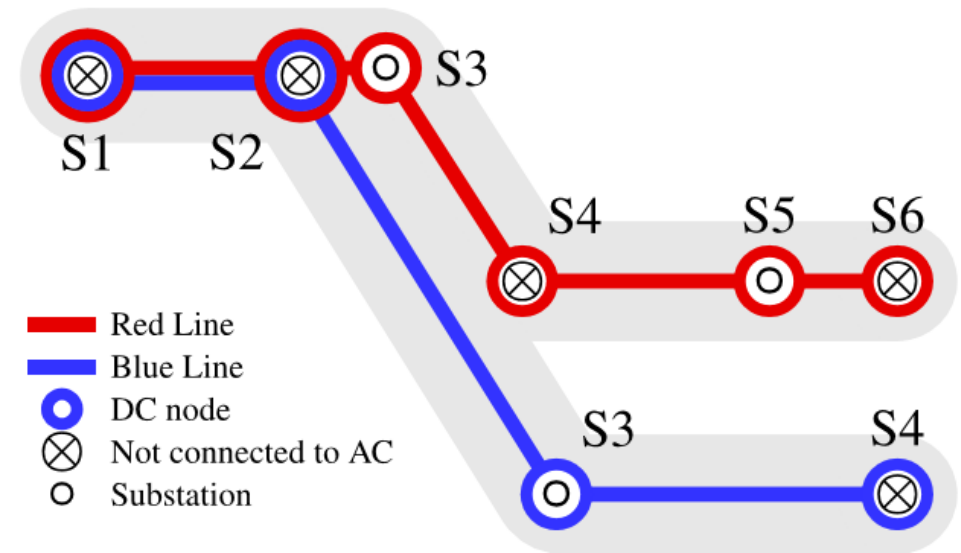
** The considered train controls are the overcurrent protection and the overvoltage protection or squeeze control

*** Trains equipped or not with on-board accumulation system

**** The substations can be conventional (non-reversible), reversible (with dead band) and non-reversible with off-board accumulation

Real Case of Study (3kV DC System)

- Red line 30.84km
- Blue line 36.93km
- Substations 3MW
- Short circuit voltage of 5%,
- No load output voltage 3kV
- Voltage at rated load (1000A) is 2880V
- Equivalent impedance in forward mode is 270m Ω
- Equivalent impedance in reverse mode 540m Ω
- Equivalent impedance of the overhead conductor and the rails (return circuit) are respectively 28.605m Ω /km and 7m Ω /km.
- Off board accumulators: 25kWh, 1MW, SOC1,2,3,4 – 0,10,90 and 100%, V1, V2, V3 and V4 will be set respectively to 2685V, 2985V, 3015V and 3315V

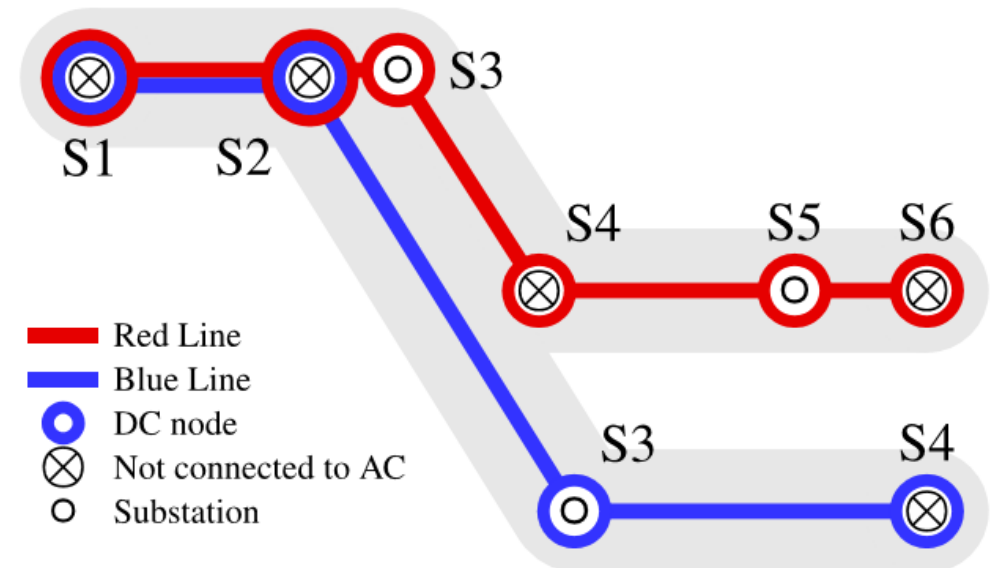


Real Case of Study (3kV DC System)

- Rolling Stock
- All EMUs, 5 cars per train
- Total unladen weight of 157.3t.
- Maximum speed 120km/h
- Maximum traction power is 2.2MW
- On-board acc. 7kWh, and 1MW.
- V1, V2, V3 and V4 (1980V, 2280V, 3300V and 3600V)

Trip	Required Mechanic. Energy	Mechanic. Regen. Capacity	Required Electrical Energy	Electrical Regen. Capacity	Min. Elect. Consump. Theoretical
S1 to S6 Red	245	112	258	106	151
S6 to S1 Red	240	107	253	102	151
S1 to S4 Blue	243	61	256	58	198
S4 to S1 Blue	187	99	197	94	103
Average Trip	229	95	241	90	151

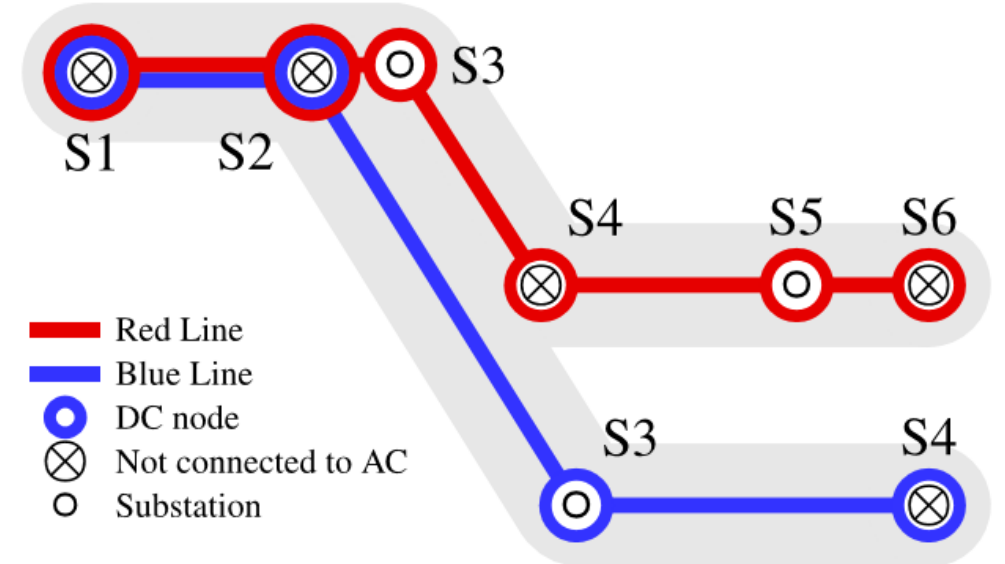
All data in kWh



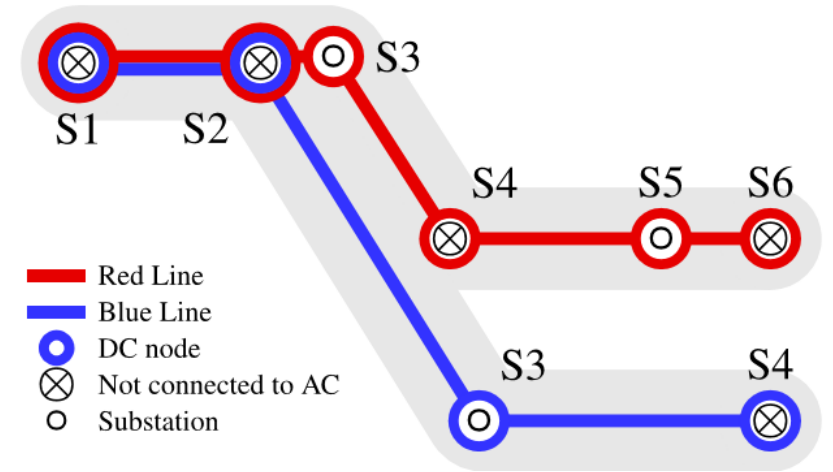
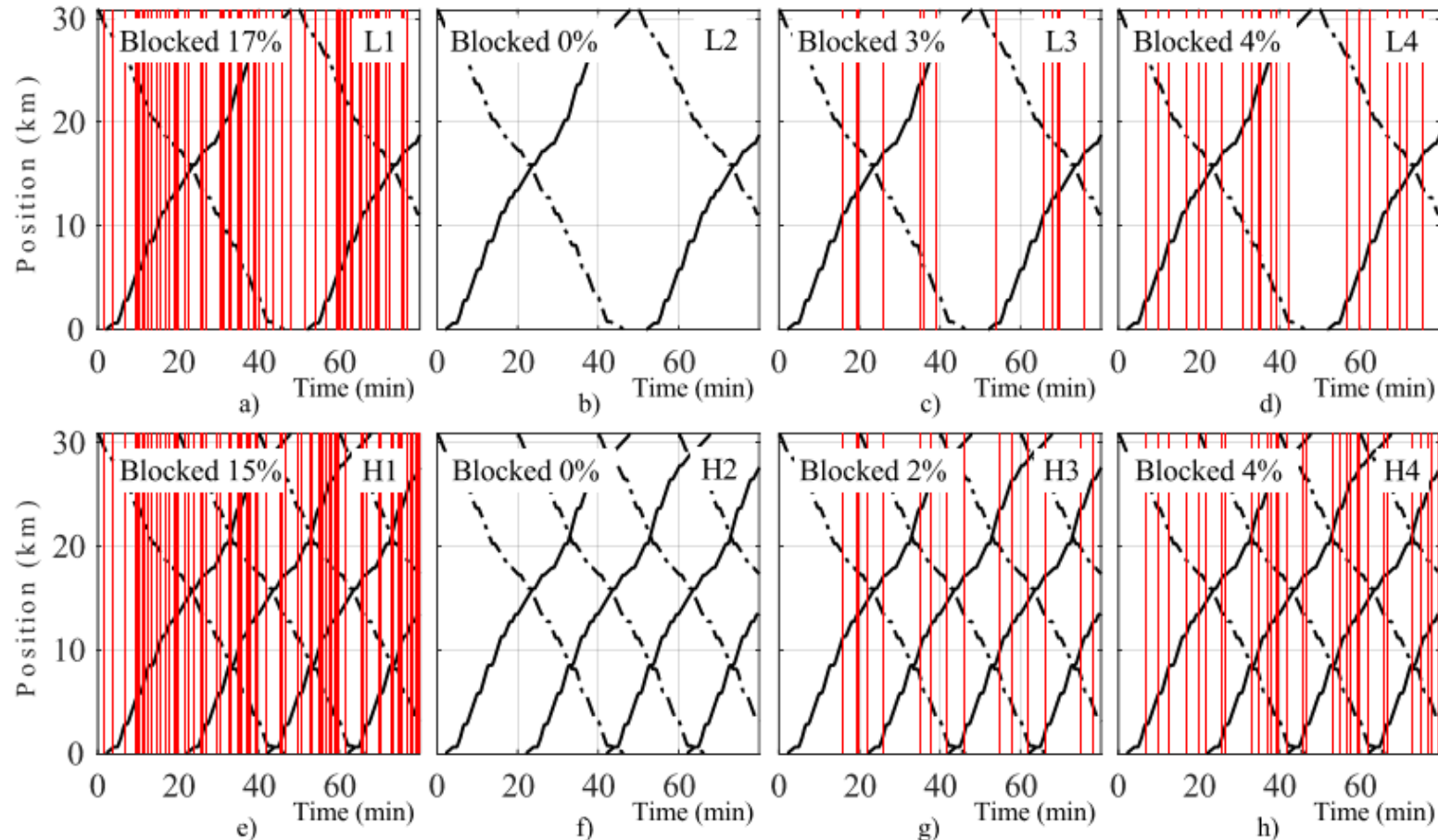
Real Case of Study (3kV DC System)

- Simulation interval about 8 hours
- Description of the scenarios:
 - 2 traffic levels

Scenario Code	Traffic Density	Revers. Subst. System	Off-board Acc.	On-board Acc.	Number of Trains	Train Headset (min)
L1	Light	No	No	No	40	50
L2	Light	Yes	No	No	40	50
L3	Light	No	Yes	No	40	50
L4	Light	No	No	Yes	40	50
H1	Heavy	No	No	No	96	20
H2	Heavy	Yes	No	No	96	20
H3	Heavy	No	Yes	No	96	20
H4	Heavy	No	No	Yes	96	20



Real Case of Study (3kV DC System)

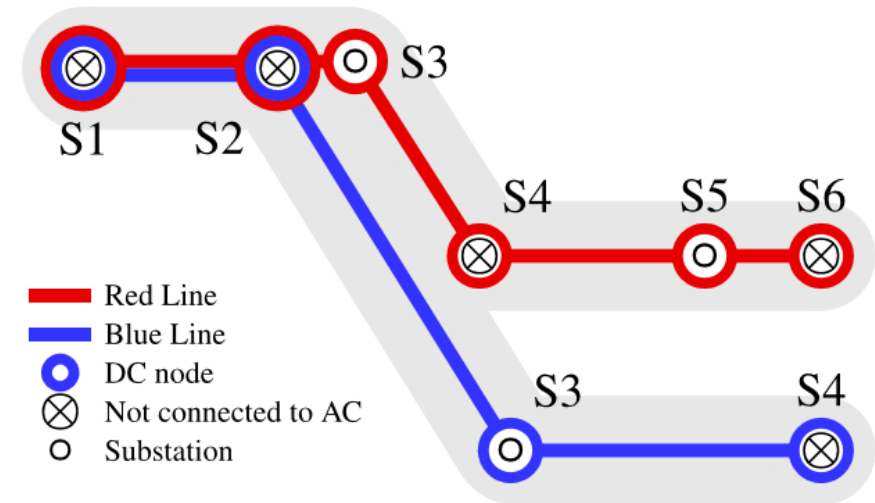


Real Case of Study (3kV DC System)

Scenario	Energy (MWh)							
	L1	L2	L3	L4	H1	H2	H3	H4
Req. Electrical	9.66	9.66	9.66	9.66	23.08	23.08	23.08	23.08
Reg. Capacity	3.62	3.62	3.62	3.62	8.65	8.65	8.65	8.65
Min. Consumpt.	6.04	6.04	6.04	6.04	14.43	14.43	14.43	14.43
Train. Demand	8.94	9.66	9.59	7.30	21.67	23.08	22.94	17.52
Train Inject.	1.61	3.62	3.26	0.58	5.93	8.65	8.26	2.00
Train Net	7.32	6.04	6.32	6.73	15.74	14.43	14.68	15.52
Rheostatic	2.01	0.00	0.36	0.49	2.72	0.00	0.39	0.79
Non Supp	0.72	0.00	0.07	0.20	1.41	0.00	0.14	0.43
Prov. Subs.	7.64	8.03	6.84	6.93	16.53	17.31	15.62	16.01
Inject. Subs.	0.0	1.69	0.0	0.0	0.0	2.13	0.00	0.0
Sub. Net	7.62	6.34	6.84	6.91	16.52	15.18	15.62	16.01
Grid Losses	0.29	0.30	0.52	0.18	0.78	0.75	0.95	0.48

System Analysis

	Energy in % respec to the electrical energy required by trains							
	L1	L2	L3	L4	H1	H2	H3	H4
Req. Electrical	100	100	100	100	100	100	100	100
Reg. Capacity	37	37	37	37	37	37	37	37
Min. Consumpt.	62	62	62	62	62	62	62	62
Train Demand	92.5	100	99.2	75.5	93.9	100	99.3	75.9
Train Inject.	16.6	37	33.7	5.9	25.7	37.4	35.8	8.6
Train Net	75.8	62.4	65.4	69.6	68.2	62.5	63.5	67.2
Rheostatic	20.8	0	3.7	5.0	11.7	0	1.6	3.4
Non Supp	7.5	0	0.7	2.0	6.0	0	0.6	1.8
Prov. Subs.	79.1	83.0	70.8	71.7	71.6	75.0	67.7	69.3
Inject. Subs.	0	17.4	0	0.1	0	9.2	0	0
Sub. Net	78.8	65.6	70.8	71.5	71.5	65.7	67.6	69.3
Grid Losses	3.0	3.1	5.3	1.9	3.3	3.2	4.1	2.0



Average Train Analysis

	Energy (kWh)							
	L1	L2	L3	L4	H1	H2	H3	H4
Train Demand	224	241	240	183	226	241	239	183
Train Inject.	40	91	82	15	62	90	86	21
Train Net	183	151	158	168	164	150	153	162
Rheostatic	50	0	9	76	28	0	4	69
Non Supp	18	0	2	4	15	0	1	3
Prov. Subs.	191	201	171	173	172	180	163	167
Inject. Subs.	0	42	0	0	0	22	0	0
Sub. Net	191	159	171	173	172	158	163	167
Grid Losses	7	8	13	5	8	8	10	5